

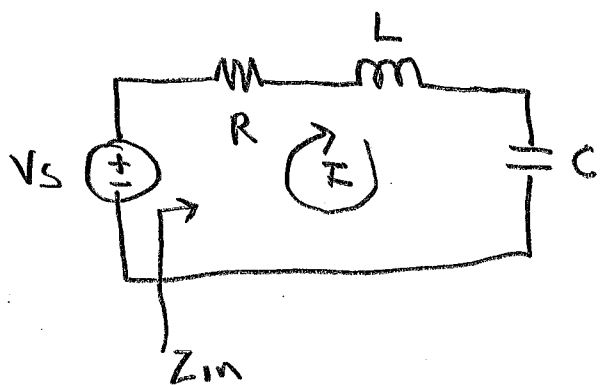
# LECTURE 19 SERIES/PARALLEL Resonance and Ladder Networks

L1

'Resonance' is characterized by a sharp peak in the amplitude vs. frequency characteristic.

"Resonance is a condition in an RLC circuit in which the capacitive and inductive reactances are equal in magnitude, thereby resulting in a purely resistive impedance"

PG-630



$$Z_{in} = Z_R + Z_L + Z_C$$

$$Z_{in} = R + j\omega L + \frac{1}{j\omega C}$$

$$Z_{in} = R + j\left(\omega L - \frac{1}{\omega C}\right)$$

Set "magnitudes of capacitive and inductive reactance to be equal"

$$\omega L - \frac{1}{\omega C} = 0 \quad \text{then} \quad Z_{in} = R$$

Solve for  $\omega_0$ .

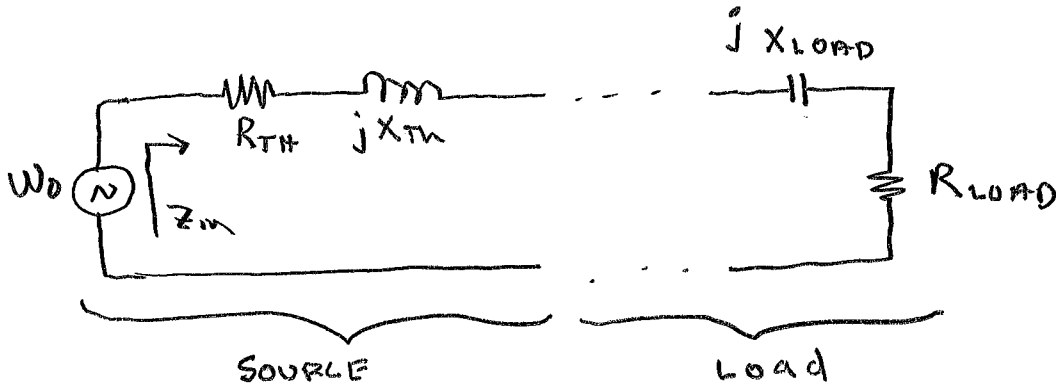
$$\omega_0 L = \frac{1}{\omega_0 C} \implies \omega_0 = \frac{1}{\sqrt{LC}}$$

At resonance (Pg 630)

ZA

- 1) Input impedance is purely resistive.
- 2) Voltage and current are in phase <sup>from supply</sup>
- 3) The magnitude of  $Z_{in}$  is minimum
- 4) The inductor and capacitor voltages can be much larger than  $V_s$

Relationship of resonance and maximum power transfer,



$$Z_{TH} = R_{TH} + jX_{TH}, \quad Z_{LOAD} = R_{LOAD} + jX_{LOAD}$$

for maximum power transfer at  $\omega_0$ ,  $Z_{LOAD} = Z_{TH}^*$

Therefore  $R_{LOAD} = R_{TH} \leftarrow$  Duh..

and  $X_{LOAD} = -X_{TH}$

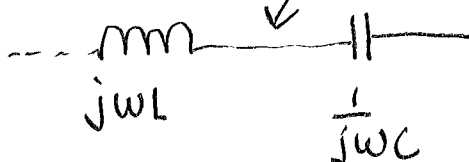
Since  $X_{TH} = \omega L$ ,  $X_{LOAD} = -\omega L = -\frac{1}{\omega C}$

capacitor needed

so  $\omega_0 L = \frac{1}{\omega C}$  and  $C = \frac{1}{\omega^2 \cdot L}$

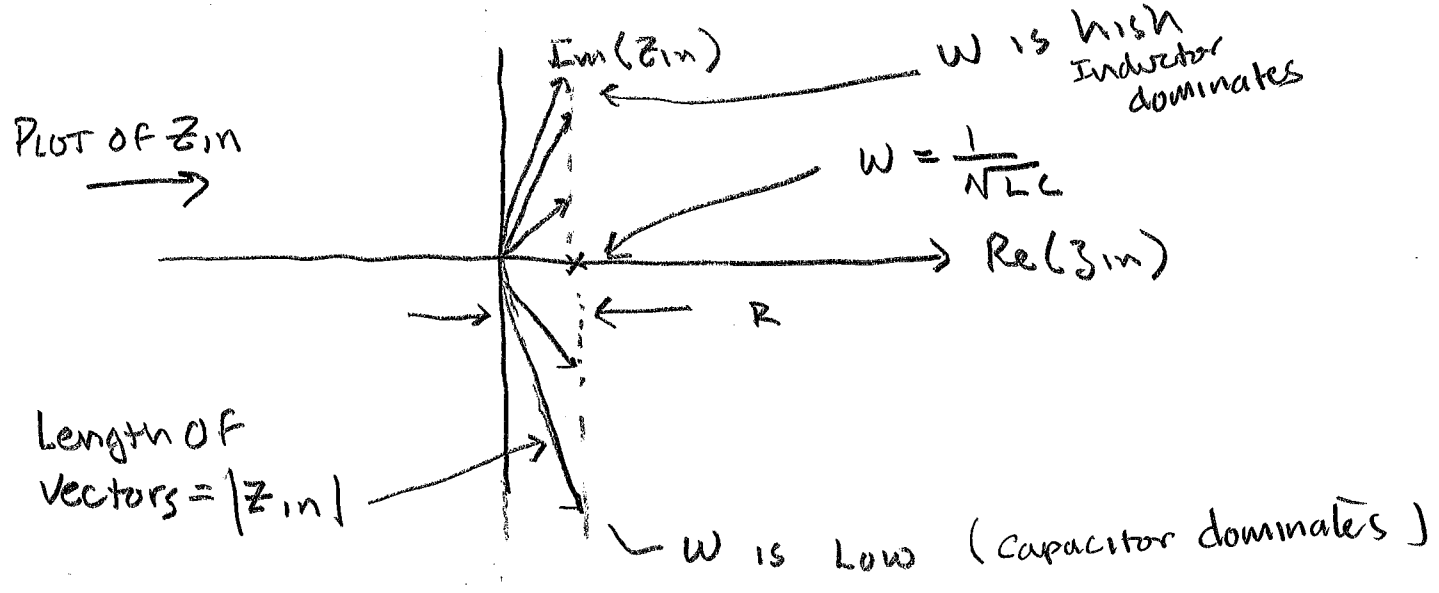
or  $\omega_0 = \frac{1}{\sqrt{LC}}$

Big voltage here



$$j\omega L + \frac{1}{j\omega C} = 0$$

PLOT  $Z_{in}$  as seen by voltage source



At  $\omega = \omega_0$  Magnitude of  $Z_{in}$  is minimized

Since  $|I| = \frac{|V_{in}|}{|Z_{in}|}$ ,  $|I|$  is maximized at  $\omega_0$

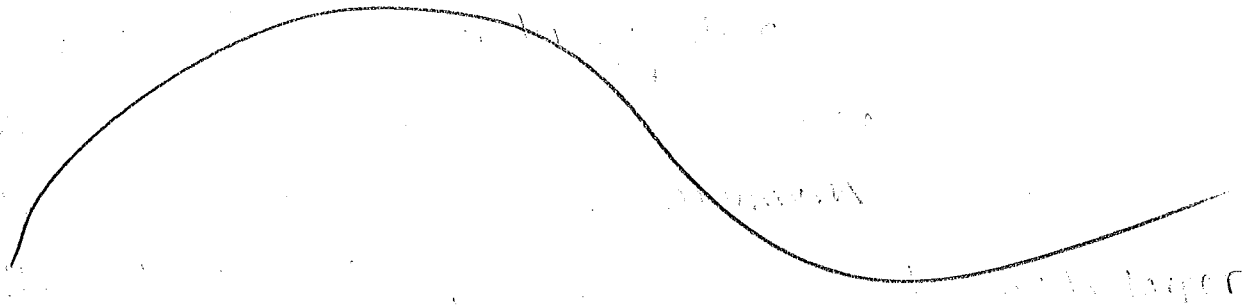
Since power in load resistor is  $\frac{1}{2} |I|^2 \cdot R$ ,

Power in load resistor is maximized at  $\omega_0$ .

How much power at  $\omega_0$ ... or max power xfer?

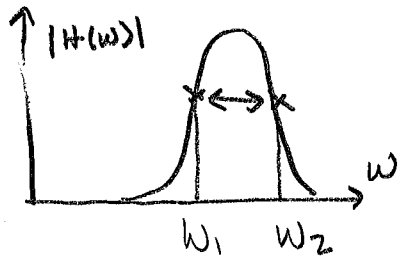
$$\frac{1}{2} |I|^2 R = \frac{1}{2} \left[ \frac{|V|}{2R} \right]^2 \times R = \frac{1}{2} \frac{|V|^2}{4R^2} \times R = \frac{|V_{in}|^2}{8R}$$

$I = \frac{V}{2R}$  ↑ EQ 11.20



Resonant circuits are characterized by their bandwidth.  
 "How wide is that peak?"

Define bandwidth as shown below



Bandwidth is  $w_2 - w_1$

$w_2$  and  $w_1$  are frequencies where circuit dissipates half the power as it does at resonance.

↑  
conceptually important

Power at resonance =  $\frac{1}{2} |I|^2 R$  at resonance

power at resonance

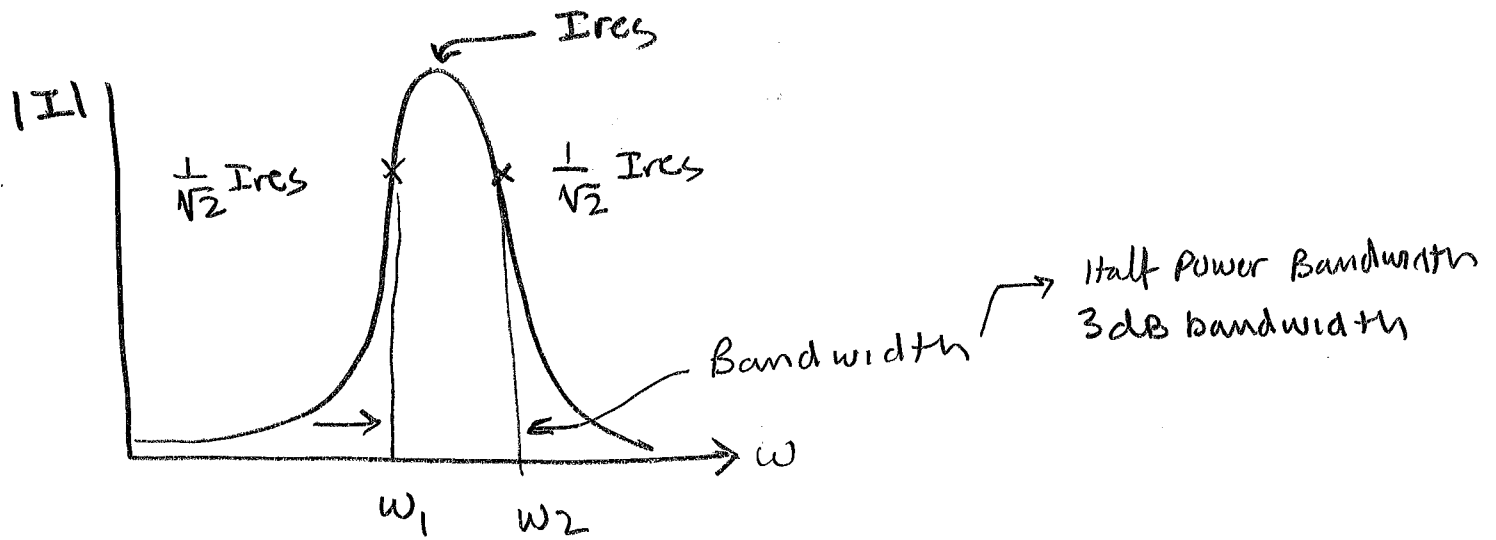
At half power frequencies, 
$$P_{resistor} = \frac{1}{2} \left[ \frac{1}{2} |I|^2 R \right] = \frac{1}{2} \left[ \frac{I}{\sqrt{2}} \right]^2 R$$

So  $w_1, w_2$  are frequencies where 
$$I = \frac{1}{\sqrt{2}} I_{resonance} = \frac{1}{\sqrt{2}} \frac{V_{in}}{R}$$

$w_1, w_2$  are also called the "3 dB frequencies"  
 or the "half-power frequencies"

From this we get the "half power" frequencies

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$$\omega_1 = -\frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

$$\omega_2 = \frac{R}{2L} + \sqrt{\left(\frac{R}{2L}\right)^2 + \frac{1}{LC}}$$

EQ 14.33

$$\omega_1 \omega_2 = \left(\frac{R}{2L}\right)^2 + \frac{1}{LC} - \frac{R^2}{4L^2} = \frac{1}{LC}$$

So  $\frac{1}{\sqrt{LC}} = \sqrt{\omega_1 \omega_2} = \omega_0$  EQ 14.34

and we see  $\omega_0$  is the geometric mean of the half-power frequencies

The "half power bandwidth" is

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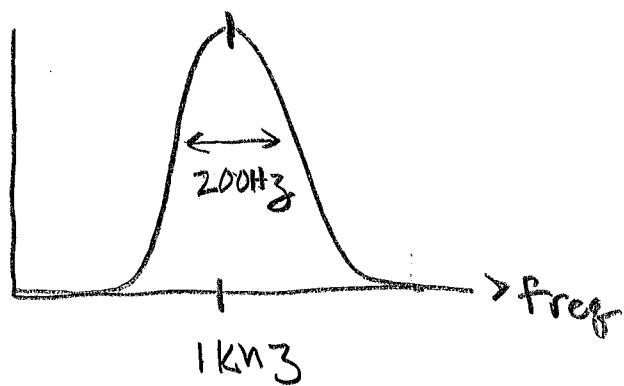
$$B = \omega_2 - \omega_1 = \frac{R}{2L} + \sqrt{\omega_c^2 - \left[ -\frac{R}{2L} + \sqrt{\omega_c^2} \right]}$$

$$B = \frac{R}{L}$$

"Quality factor" =  $Q = \frac{\omega_0 L}{R} = \frac{1}{\omega_0 RC}$  EQ 14.38

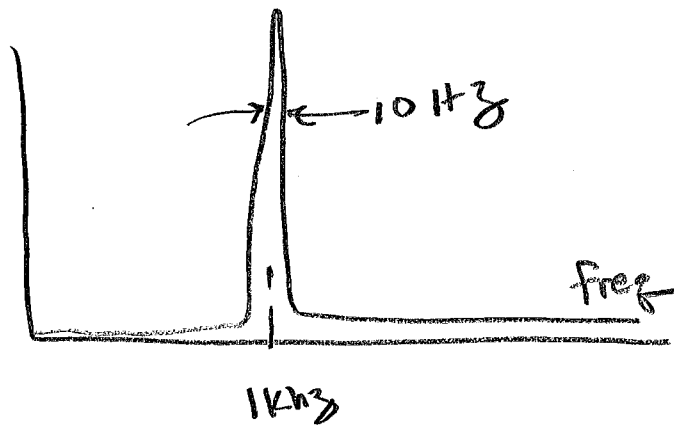
OR  $B = \frac{\omega_0}{Q}$  EQ 14.39

Bandwidth in  $r/s = \frac{\omega_0}{Q}$ , Bandwidth in Hz =  $\frac{f_0}{Q}$



$$Q = \frac{1 \text{ kHz}}{200 \text{ Hz}} = 5$$

"Low Q"



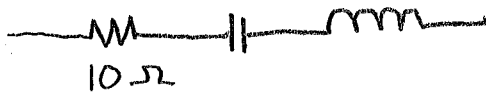
$$Q = \frac{1 \text{ kHz}}{10 \text{ Hz}} = 100$$

"High Q"

Which filter is "more selective?"

PR 14.28

Design a series resonant circuit with  $BW = 20 \text{ r/s}$   
and  $\omega_0 = 1000 \text{ r/s}$ . Find  $Q$ . Let  $R = 10 \Omega$



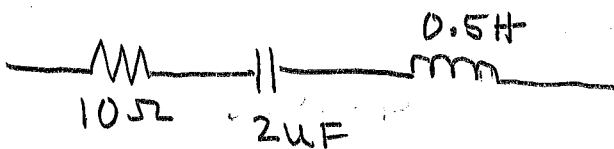
$$BW = 20 \text{ r/s} = \frac{R}{L} = \frac{\omega_0}{Q} \quad \text{EQ 14.38}$$

$$\text{so } L = \frac{R}{20} = \frac{10}{20} = \frac{1}{2} \text{ H}$$

$$\omega_0 = \frac{1}{\sqrt{LC}} \quad \text{EQ 14.26}$$

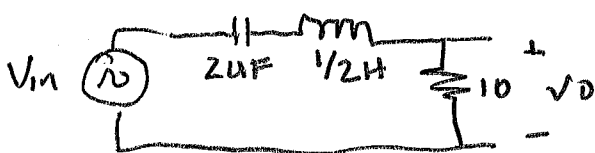
$$\text{so } \omega_0^2 LC = 1 \quad \text{or } C = \frac{1}{\omega_0^2 L} = \frac{1}{1000^2 \times 0.5}$$

$$\text{and } Q = \frac{\omega_0 L}{R} = \frac{1000 \times 0.5}{10} = 50 = 2 \mu\text{F}$$



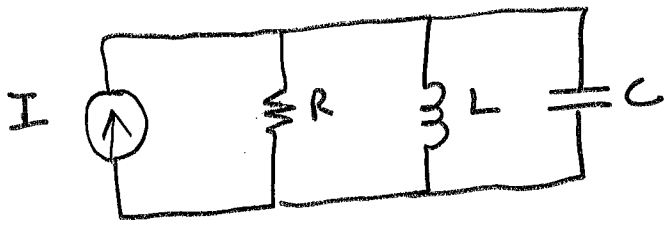
check...

$$\omega_0 = \frac{1}{\sqrt{LC}} = 1000 \text{ r/s} \quad BW = \frac{R}{L} = 20 \text{ r/s} \quad Q = \frac{\omega_0}{BW} = \frac{1000}{20} = 50$$



What is  $\frac{V_o}{V_{in}}$  at  $\omega = \omega_0$ ?

# Parallel resonance

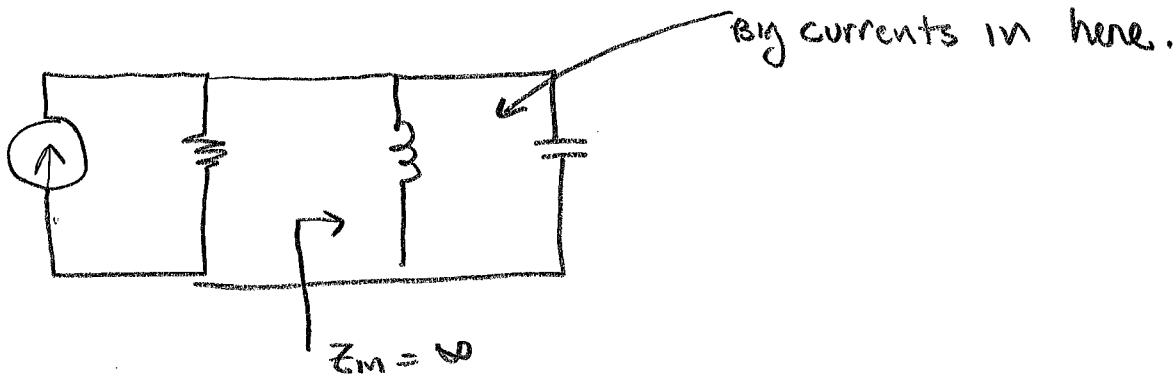


At resonance  $Y_C = -Y_L$   
 or  $j\omega_0 C = -\frac{1}{j\omega_0 L} = \frac{j}{\omega_0 L}$

Solving  $\omega_0 C = \frac{1}{\omega_0 L}$  or  $\omega_0 = \frac{1}{\sqrt{LC}}$

Since  $Y_C + Y_L = 0$ , impedance of parallel

combination is  $\frac{1}{Y_T} = \frac{1}{0} = \infty$



$$\omega_1 = -\frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC}\right)^2 + \frac{1}{LC}}, \quad \omega_2 = \frac{1}{2RC} + \sqrt{\left(\frac{1}{2RC}\right)^2 + \frac{1}{LC}}$$

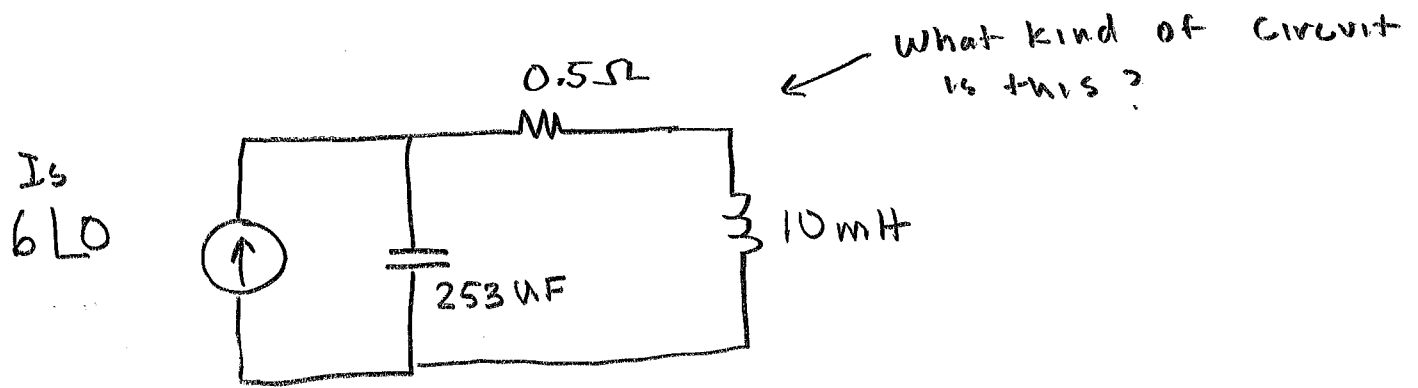
$$BW = \omega_2 - \omega_1 = \frac{1}{RC}, \quad Q = \frac{\omega_0}{B} = \omega_0 RC = \frac{R}{\omega_0 L}$$

Parallel is different than series!



# Example

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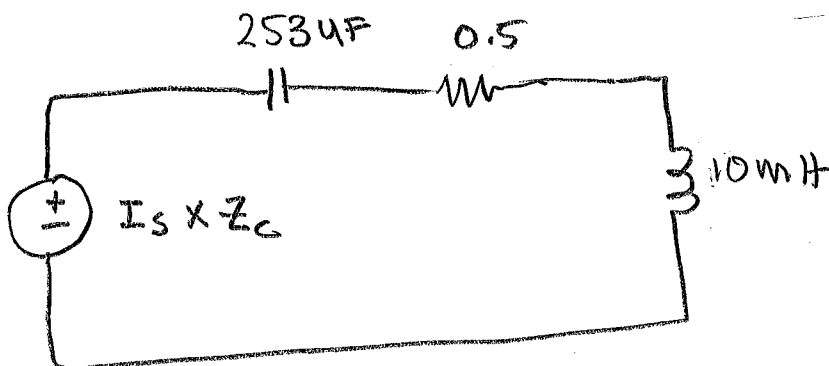
Find resonant frequency in Hz

Find bandwidth in Hz

Find Q

Find power dissipated in 0.5 Ω at resonance

find power dissipated in 0.5 Ω at lower 3 dB frequency



$$f_0 = \frac{1}{2\pi} \times \frac{1}{\sqrt{LC}} = 100 \text{ Hz} \quad \text{EQ 14.26}$$

$$BW = \frac{1}{2\pi} \frac{R}{L} = \frac{1}{2\pi} \times \frac{0.5}{0.01} = 7.96 \text{ Hz} \quad \text{EQ 14.39}$$

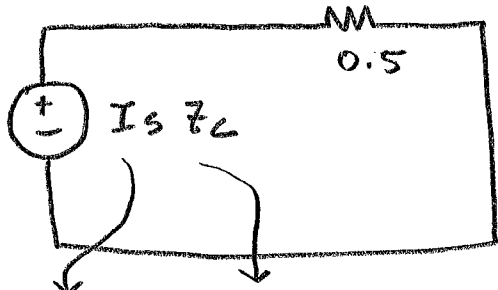
$$Q = \frac{f_0}{BW} = \frac{100}{7.96} = 12.5$$

↳ r/s or Hz as long as they are the same

CONT →

Find power dissipated in the  $0.5 \Omega$  resistor at resonance

At resonance  $Z_C + Z_L = 0$  so current is computed using the equivalent circuit



$$6 \angle 0 \times \frac{1}{j2\pi \times 100 \times 253 \mu\text{F}} = -j37.74 \text{ V}$$

↑  
resonant frequency

$$P = \frac{1}{2} \frac{V_m^2}{R} = \frac{1}{2} \times \frac{37.74^2}{0.5} = 1424.3 \text{ W}$$

Find the power dissipated in the  $0.5 \Omega$  resistor at the lower 3 dB frequency.

- Use EQ 4.31 for series resonance

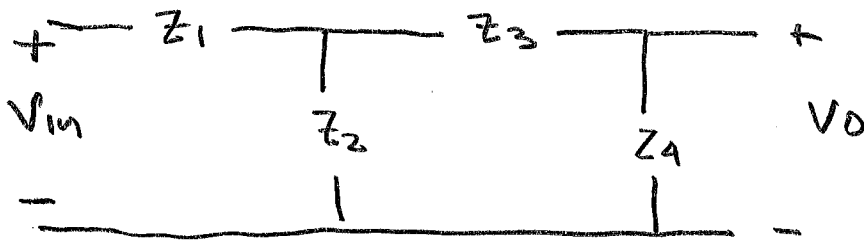
$$P = \frac{V_m^2}{4R} = \frac{37.74^2}{4 \times 0.5} = 712.1 \text{ W}$$

- OR note that at the 3 dB (half power) frequencies the current is  $1/\sqrt{2}$  times the peak current and

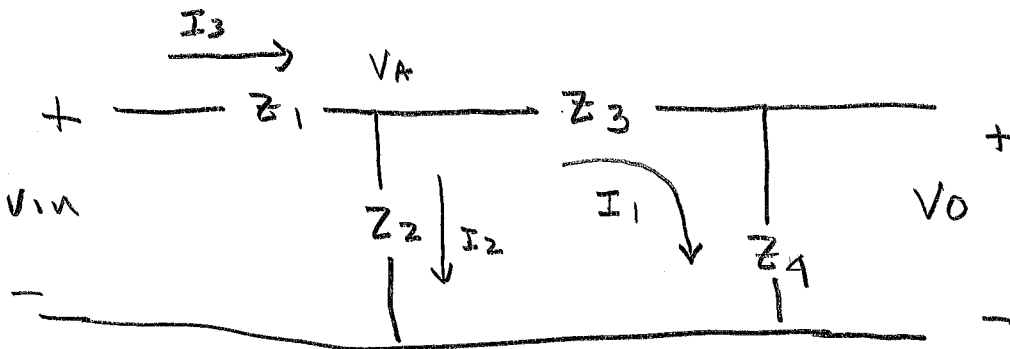
$$\frac{P_{3dB}}{P_{res}} = \frac{\frac{1}{2} |1/\sqrt{2} I_m|^2 R}{\frac{1}{2} |I_m|^2 R} = \frac{1}{2}$$

# LADDER NETWORKS

Find  $V_0/V_{in}$



Strategies?



Set output to  $1 \angle 0^\circ$  V, compute input then  $\frac{V_0}{V_{in}} = \frac{1 \angle 0^\circ}{V_{in}(\angle)}$

$$I_1 = \frac{1}{Z_4}$$

$$V_A = 1 + I_1 Z_3$$

$$I_2 = \frac{V_A}{Z_2}$$

$$I_3 = I_1 + I_2$$

$$V_{in} = V_A + I_3 Z_1$$

Compute, Substitute, Compute . . . .

$$\frac{V_0}{V_{in}} = \frac{1 \angle 0}{V_{in}}$$

$$I_1 = \frac{1}{Z_4}$$

$$V_A = 1 + I_1 Z_3 = 1 + \frac{Z_3}{Z_4}$$

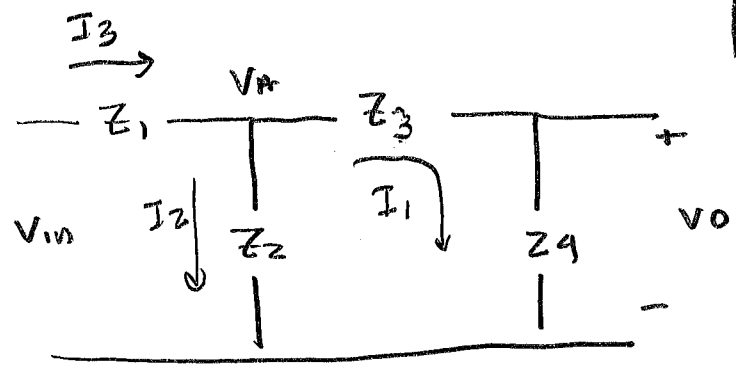
$$I_2 = \frac{V_A}{Z_2} = \frac{1 + \frac{Z_3}{Z_4}}{Z_2}$$

$$I_3 = I_1 + I_2 = \frac{1}{Z_4} + \frac{1 + \frac{Z_3}{Z_4}}{Z_2}$$

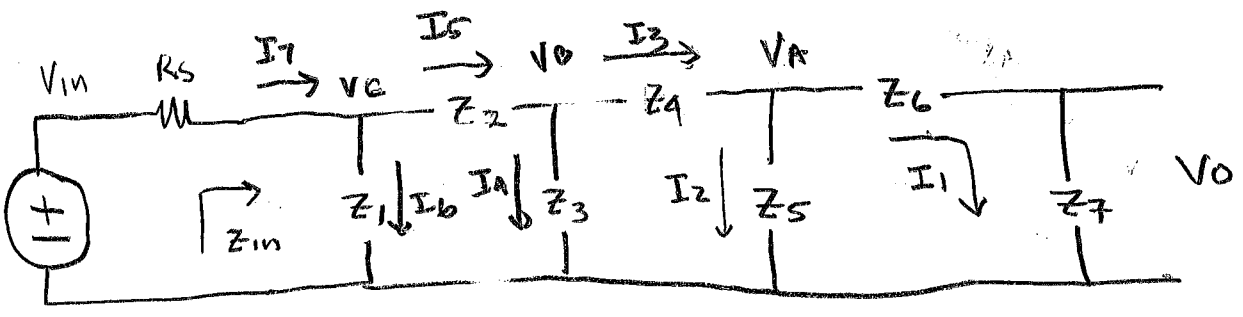
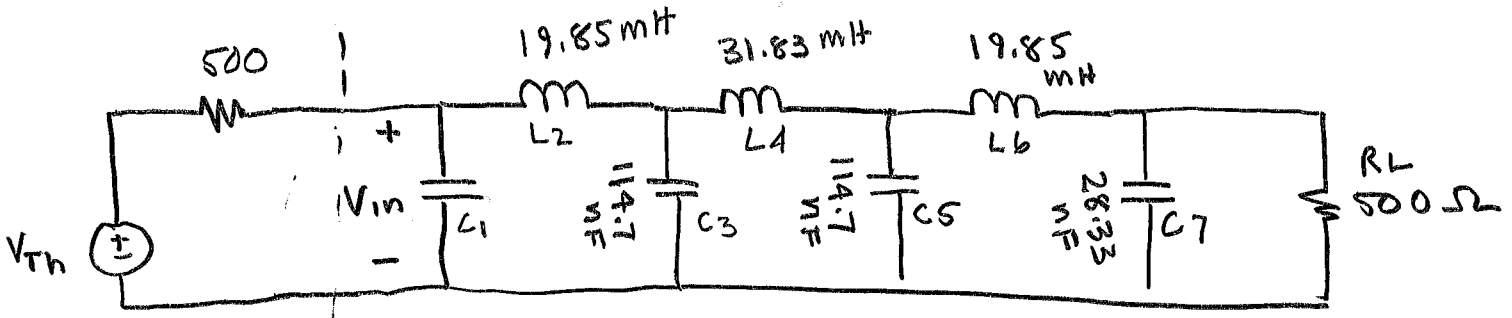
$$V_{in} = V_A + I_3 Z_1 = \underbrace{1 + \frac{Z_3}{Z_4}}_{V_A} + \underbrace{\left[ \frac{1}{Z_4} + \frac{1 + \frac{Z_3}{Z_4}}{Z_2} \right]}_{I_3} Z_1$$

$$\frac{V_o}{V_{in}} = \frac{1}{1 + \frac{Z_3}{Z_4} + \left[ \frac{1}{Z_4} + \frac{1 + \frac{Z_3}{Z_4}}{Z_2} \right] Z_1}$$

What's so easy about this?



EXAMPLE



```

clear all;
close all;

% Specify components.
Rs = 500;
C1 = 28.33e-9;
C3 = 114.7e-9;
C5 = 114.7e-9;
C7 = 28.33e-9;
L2 = 19.85e-3;
L4 = 31.83e-3;
L6 = 19.85e-3;
R1 = 500;

StartFreq = 10;      % Lowest frequency to plot.
NumDec = 4;          % Number of decades to plot.
PtsPerDec = 200;    % Number of frequency points plotted per decade.

% Pre-allocate results matrices.
MagResp = zeros(NumDec*PtsPerDec,1); % Matrix containing magnitude response.
Freq = zeros(NumDec*PtsPerDec,1);    % Matrix containing plot frequencies.

% Compute frequency response at frequency points uniformly-spaced on a log plot.
for i=1 : NumDec*PtsPerDec
    Freq(i) = StartFreq*10^(i/PtsPerDec); % Evaluate at this frequency.
    s = 1j * 2*pi*Freq(i);                % Determine complex frequency.

    % Compute branch impedances at this frequency.
    Z1 = 1/(s*C1);
    Z2 = s*L2;
    Z3 = 1/(s*C3);
    Z4 = s*L4;
    Z5 = 1/(s*C5);
    Z6 = s*L6;
    Z7 = (1/(s*C7) * R1) / (1/(s*C7) + R1);

    Vo = 1;
    I1 = 1/Z7;
    Va = 1 + I1*Z6;
    I2 = Va/Z5;
    I3 = I1 + I2;
    Vb = Va + I3*Z4;
    I4 = Vb/Z3;
    I5 = I3 + I4;
    Vc = Vb + I5*Z2;
    I6 = Vc/Z1;
    I7 = I5 + I6;
    Vin = Vc + I7 * Rs;

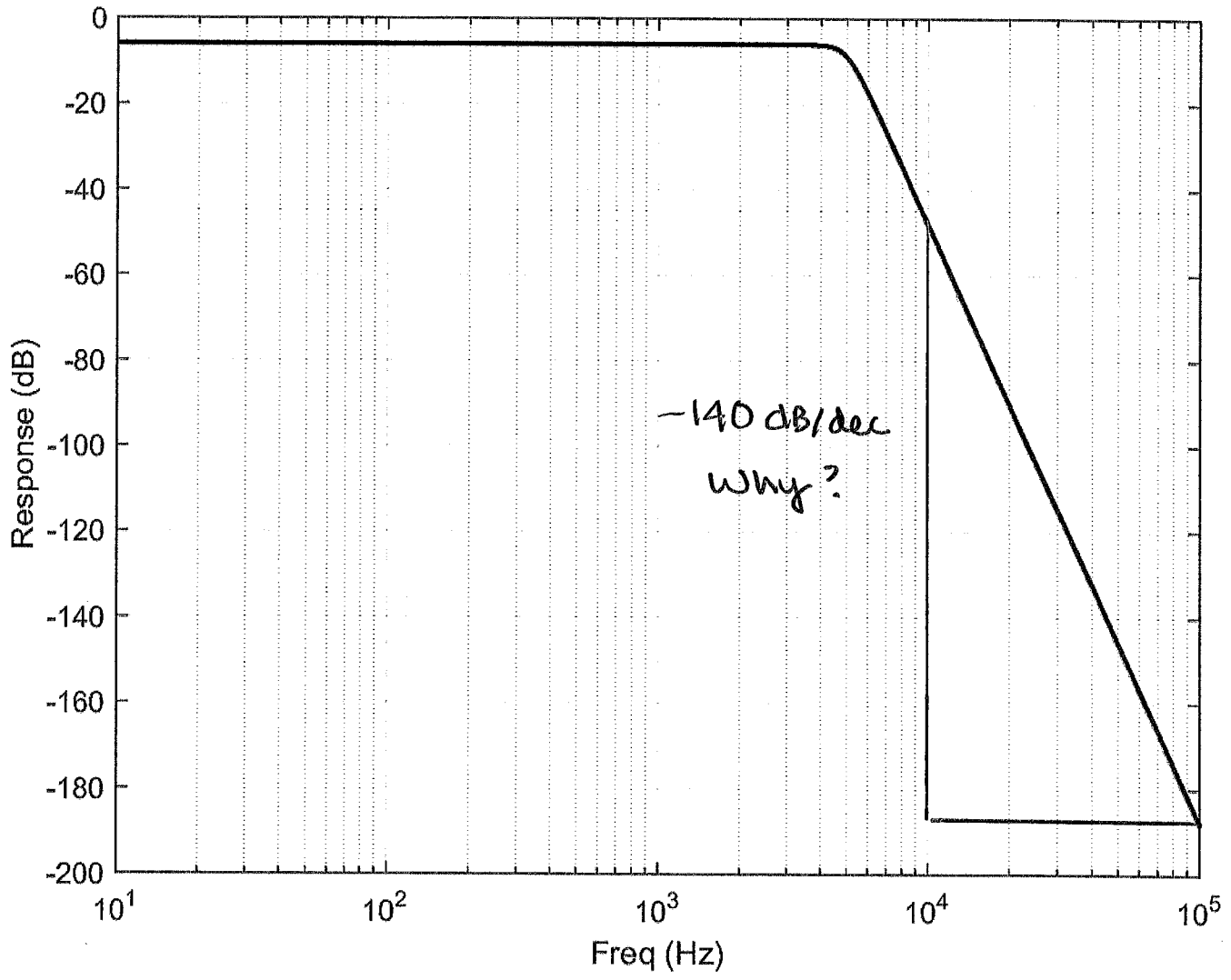
    H = Vo/Vin;

```

```
MagResp(i) = abs(H);    % Place magnitude response in result matrix.
end

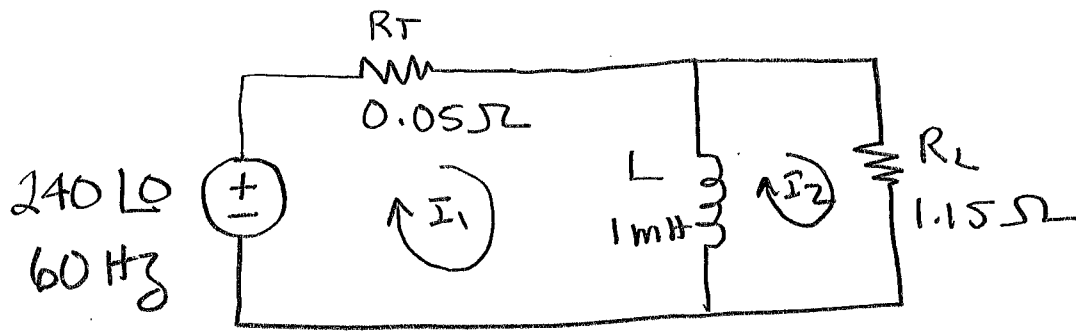
% Plot magnitude.
HMag=semilogx(Freq,20*log10(MagResp), 'color','k', 'linewidth', 2); % Plot magnitude

set(gca,'FontSize',12);
xlabel('Freq (Hz)');
ylabel('Response (dB)');
% ylim([-50, 10]);
grid on;
```





# EXAMPLE



Determine power delivered to  $R_T$  and  $R_L$

Strategy: Use mesh analysis to get currents in  $R_T$  and  $R_L$

$$P_{WR}(R_T) = \frac{1}{2} I_{1m}^2 R_T$$

$$P_{WR}(R_L) = \frac{1}{2} I_{2m}^2 R_L$$

$$\textcircled{1} -240 + I_1 R_T + (I_1 - I_2) j\omega L = 0$$

$$(R_T + j\omega L) I_1 - j\omega L I_2 = 240$$

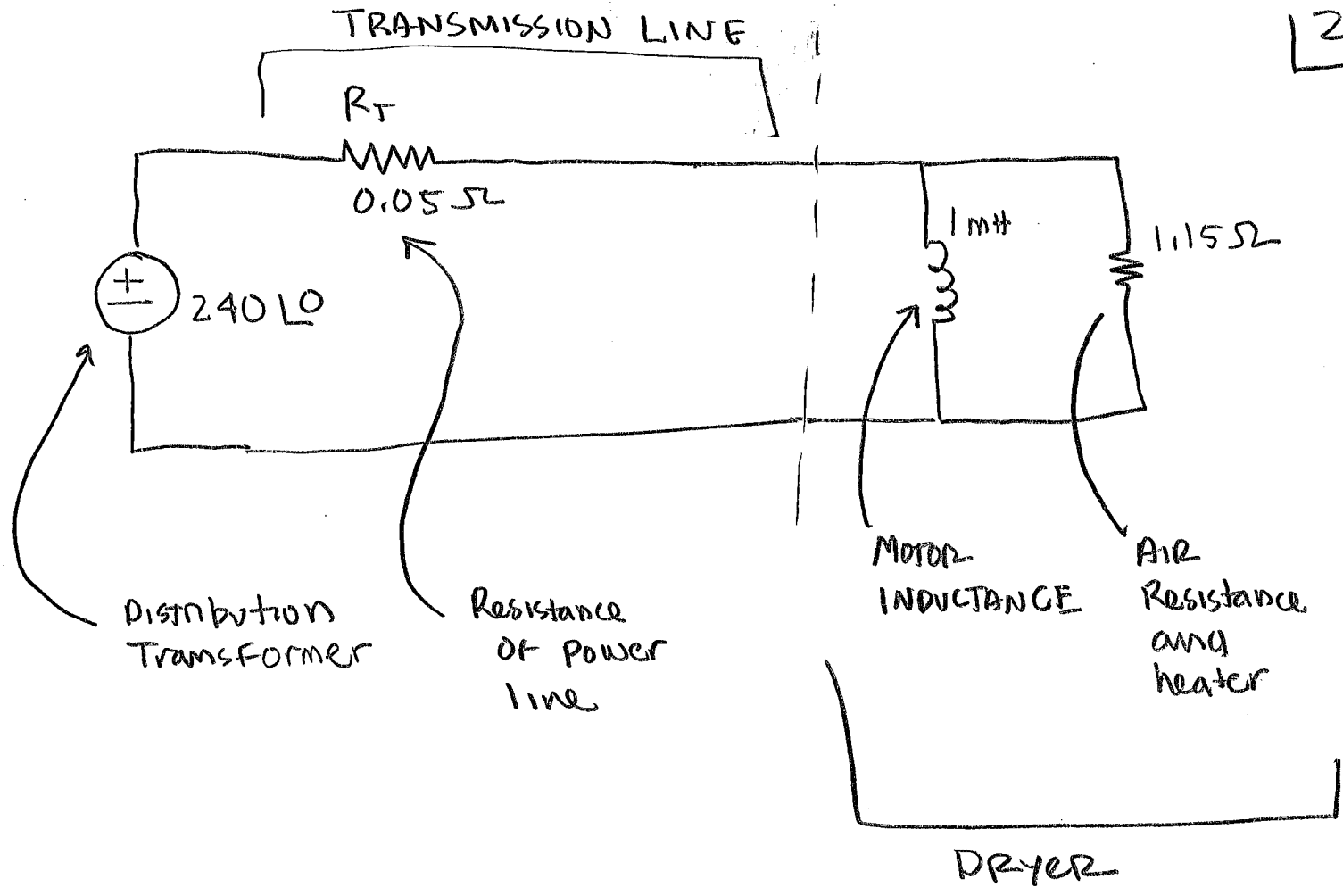
$$\textcircled{2} (I_2 - I_1) j\omega L + I_2 R_L = 0$$

$$-j\omega L \cdot I_1 + (j\omega L + R_L) I_2 = 0$$

$$\begin{bmatrix} R_T + j\omega L & -j\omega L \\ -j\omega L & j\omega L + R_L \end{bmatrix}^{-1} \begin{bmatrix} 240 \\ 0 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{matrix} 636.9 \angle -64.6^\circ \\ 198.4 \angle 7.24^\circ \end{matrix}$$

$$\text{SO } P(R_T) = \frac{1}{2} |I_1|^2 \times R_T = \frac{1}{2} \times (636.9)^2 \times 0.05 = 10.14 \text{ KW}$$

$$P_{R_L} = \frac{1}{2} |I_2|^2 \times R_L = \frac{1}{2} (198.4)^2 \times 1.15 = 22.63 \text{ KW}$$

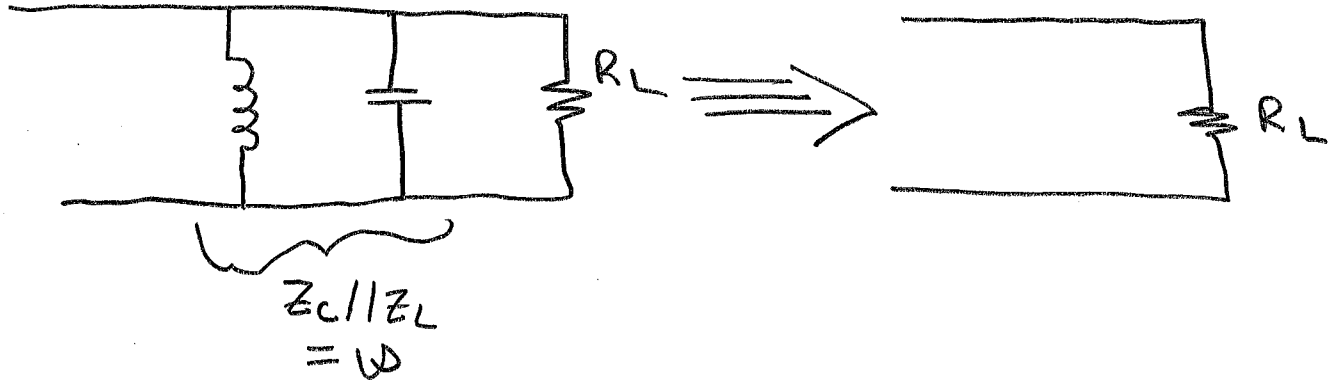


The power company pays for power in  $R_T$

The customer pays for the power in  $R_L$

So the power company places a capacitor at the car wash.

Pick capacitor so  $Z_C \parallel Z_L = \infty$



Set  $Z_C // Z_L$  to  $\infty$

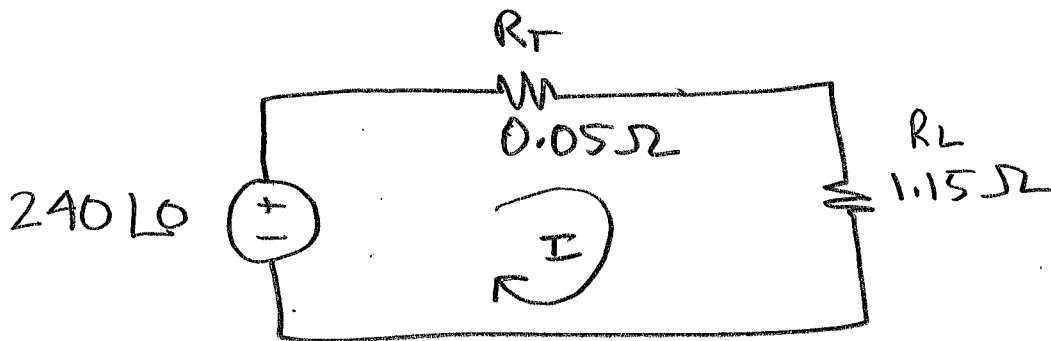
3

$$\frac{\frac{1}{j\omega C} \times j\omega L}{\frac{1}{j\omega C} + j\omega L} = \frac{L/C}{\underbrace{-\frac{j}{\omega C} + j\omega L}} = \infty$$

Den must be zero so

$$\frac{1}{\omega C} = \omega L \quad \text{or} \quad C = \frac{1}{\omega^2 L} = \frac{1}{(2\pi \times 60)^2 \times 0.001}$$
$$= 7.036 \mu\text{F}$$

Now we have



$$I = \frac{240}{0.05 + 1.15} = 200 \text{ A}$$

$$P_{RT} = \frac{1}{2} |I|^2 R_T = \frac{1}{2} \times 200^2 \times 0.05 = 1000 \text{ W}$$

$$P_{RL} = \frac{1}{2} |I|^2 R_L = \frac{1}{2} \times 200^2 \times 1.15 = 23.0 \text{ kW}$$

	TOTAL	$R_T$	$R_L$	% of total in $R_L$
NO CORR	32.8 KW	10.14 KW	22.63	69% <span style="border: 1px solid black; padding: 2px;">4</span>
CORR	24.0 KW	1 KW	23.0 KW	96%

What's going on?

- 1) Inductive part of load is an energy storage device.
- 2) Inductor accepts energy from source, then throws it back.
- 3) Whenever energy goes across power line, some is lost in the resistance  $R_T$ . Power company must pay!
- 4) The parallel capacitor makes the load site purely resistive (Energy is transferred between inductor and capacitor)

"Power factor correction - EE 310 style"