

LECTURE 13 - MUTUAL INDUCTANCE

- Conductively coupled circuits
- Magnetically coupled circuits

Why?

- Electrical isolation
- Step up/down for voltages and currents
- Impedance matching for maximum power transfer
- Filters!!

Introduction

Electricity and magnetism are related by Maxwell's equations.

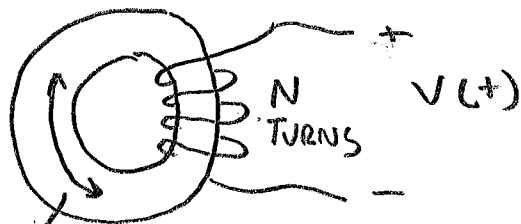
For our purposes we simplify to Faraday's Law:

$$V(t) = N \frac{d\phi}{dt}$$

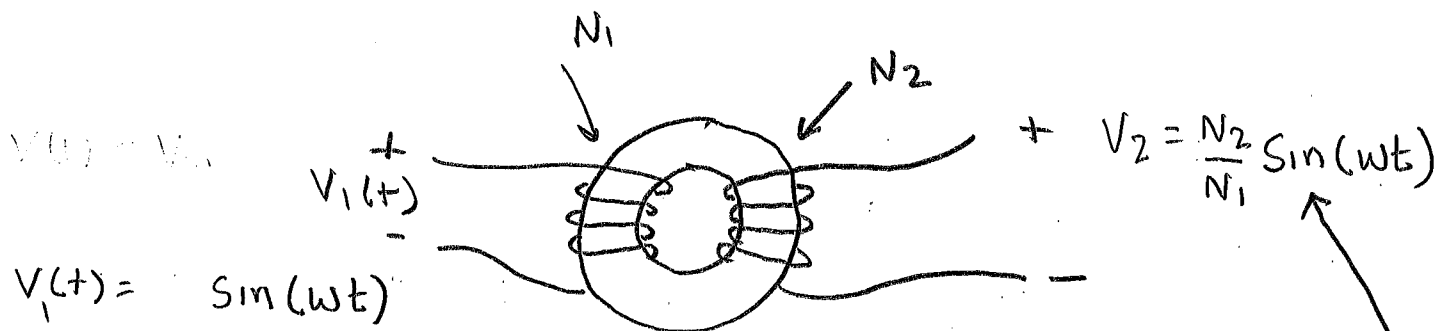
change in flux through a surface.

Flux can induce voltage,

Voltage can induce flux,



Flux, ϕ , is in core.



$$\phi(t) = \frac{1}{N_1} \int \sin(wt) dt$$
$$V_2 = N_2 \frac{d\phi}{dt} = \frac{N_2}{N_1} \sin(wt)$$

- Ideal transformer will be introduced in sec 13.5
- Not all of the flux is coupled by both coils, some leaks out

We start with

$$V(t) = N \frac{d\phi}{dt}$$

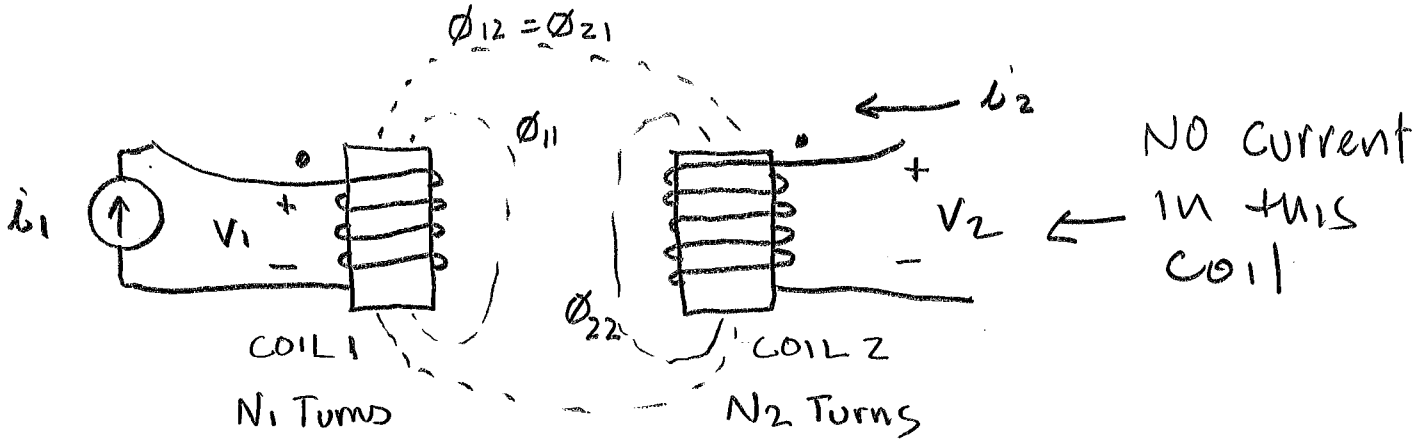
But, Flux is produced by current

so we have

$\frac{d\phi}{dt}$ is flux change with a single turn

$$V(t) = N \frac{d\phi}{dt} = N \frac{d\phi}{di} \cdot \frac{di}{dt} = L \frac{di}{dt}$$

INDUCTANCE



Flux from coil 1 = $\phi_1 = \phi_{11} + \phi_{12}$

$$V_1 = N_1 \frac{d\phi_1}{dt} = N_1 \frac{d\phi_1}{di_1} \cdot \frac{di_1}{dt} = L_1 \frac{di_1}{dt} \quad \text{EQ 13.8}$$

self inductance of coil 1

$$V_2 = N_2 \frac{d\phi_{12}}{dt} = N_2 \frac{d\phi_{12}}{di_1} \cdot \frac{di_1}{dt} = M_{21} \frac{di_1}{dt} \quad \text{EQ 13.11}$$

Mutual inductance

We could place current source on the right side and get

$$V_2 = L_2 \frac{di_2}{dt} \quad \text{EQ 13.13}$$

and

$$V_1 = M_{12} \frac{di_2}{dt} \quad \text{EQ 13.15}$$

My Favorite equations:

$$V_1 = L_1 \frac{di_1}{dt} + M_{21} \frac{di_2}{dt}$$

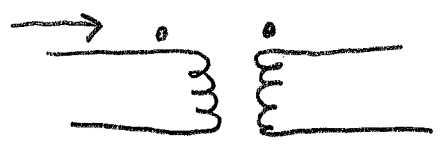
$$V_2 = L_2 \frac{di_2}{dt} + M_{12} \frac{di_1}{dt}$$

$$M_{12} = M_{21}$$

So "Mutual inductance is the ability of one inductor to induce a voltage across a neighboring inductor measured in Henries"

← Bottom of Pg 538

DOTS — Connecting the physical part with the math



"If a current enters the dotted terminal of one coil, the reference polarity of the mutual voltage in the second coil is positive at the dotted terminal of the second coil"

← Pg 559

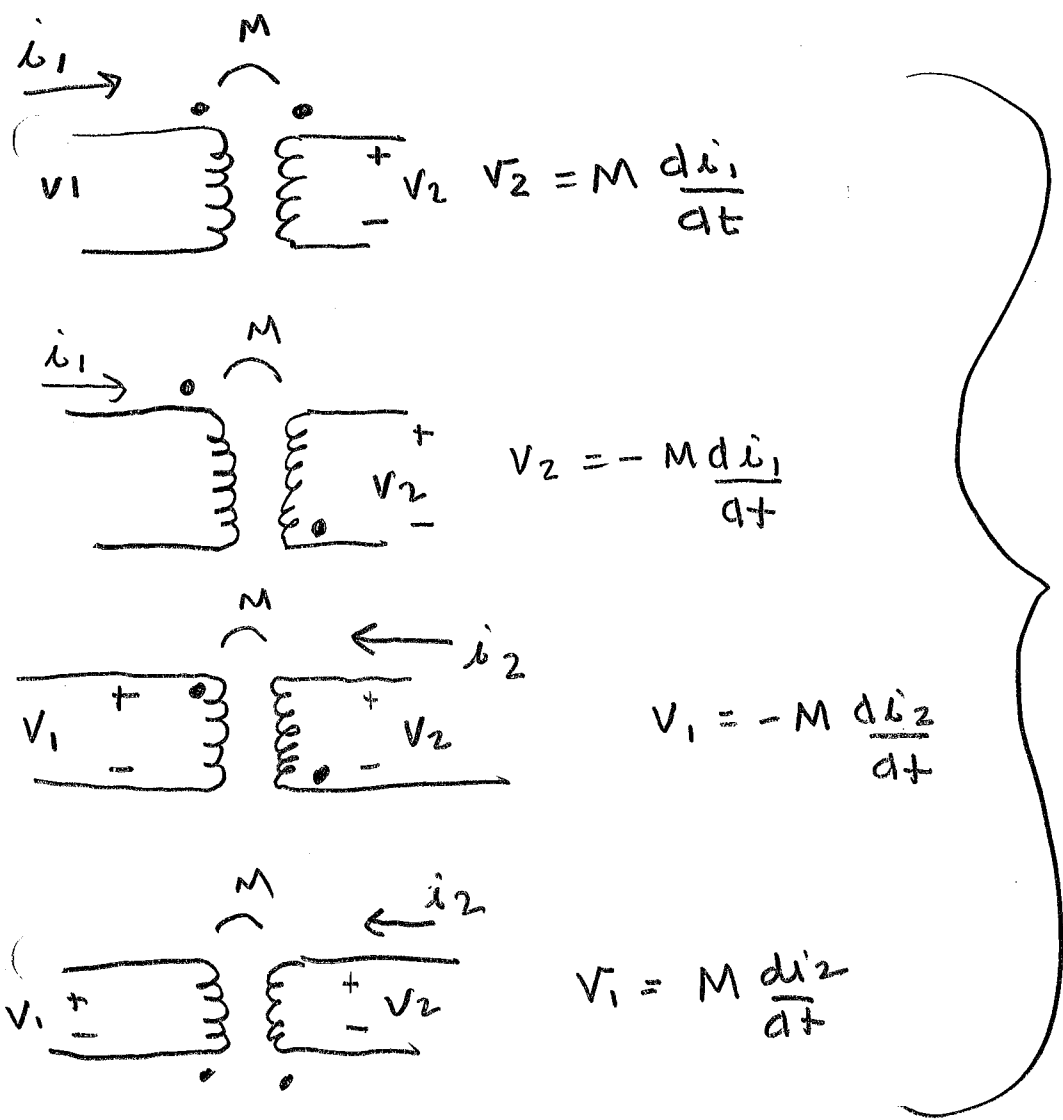
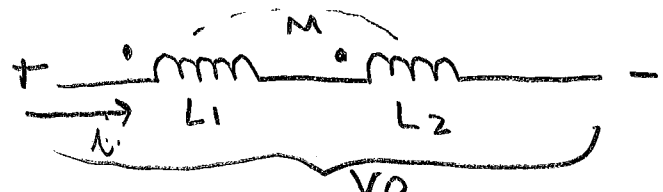


Fig 13.5
IN Text

COUPLED COILS IN SERIES

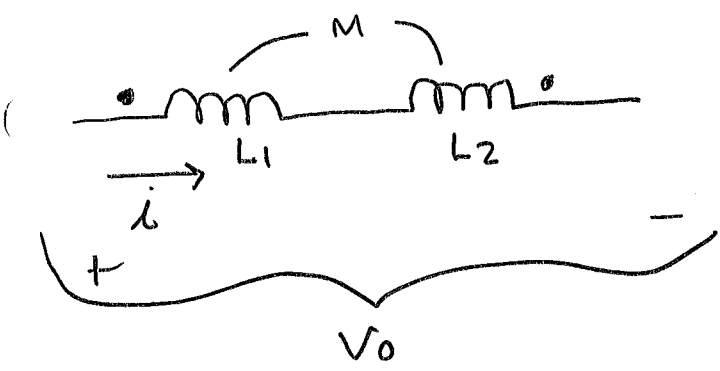


IF NOT COUPLED, $L_s = L_1 + L_2$

IF COUPLED, USE KVL

$$V_0 = L_1 \frac{di}{dt} + \underset{\substack{\uparrow \\ \text{induced in} \\ \text{coil 2}}}{M \frac{di}{dt}} + L_2 \frac{di}{dt} + \underset{\substack{\uparrow \\ \text{induced} \\ \text{in coil 1}}}{M \frac{di}{dt}}$$

$$V_0 = (L_1 + L_2 + 2M) di/dt \quad \text{so } L_s = L_1 + L_2 + 2M \rightarrow \text{EQ 13.8}$$



$$V_0 = L_1 \frac{di}{dt} - M \frac{di}{dt} + L_2 \frac{di}{dt} - M \frac{di}{dt}$$

$$V_0 = (L_1 + L_2 - 2M) \frac{di}{dt}$$

So $L_s = L_1 + L_2 - 2M$ EQ 13.19

Housekeeping to make problems easier - pg 561

$$V_1 = L_1 \frac{di_1}{dt} + M \frac{di_2}{dt} = j\omega L_1 I_1 + j\omega M I_2$$

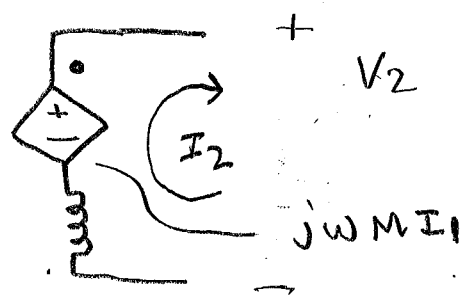
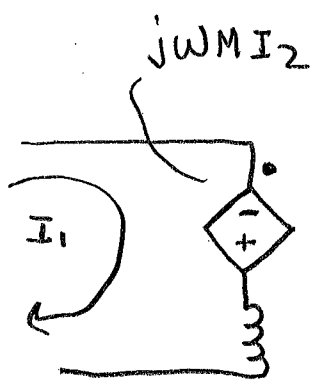
$$V_2 = L_2 \frac{di_2}{dt} + M \frac{di_1}{dt} = j\omega L_2 I_2 + j\omega M I_1$$

differential

Phasor

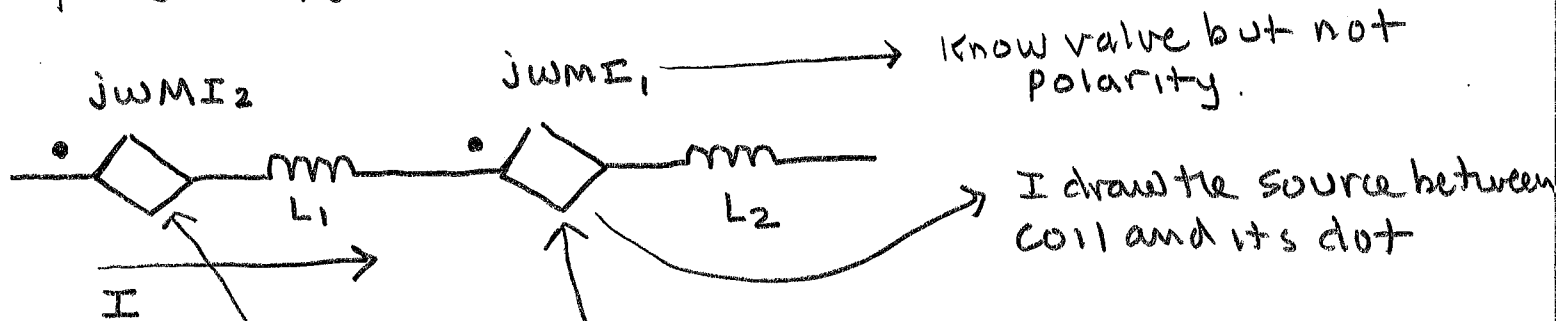
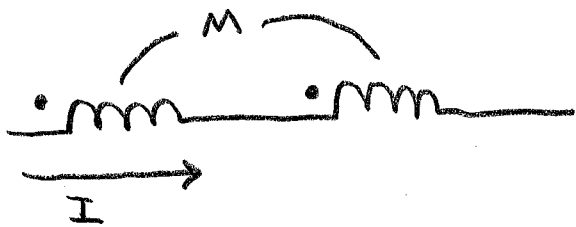
Regular Inductor

dependent source



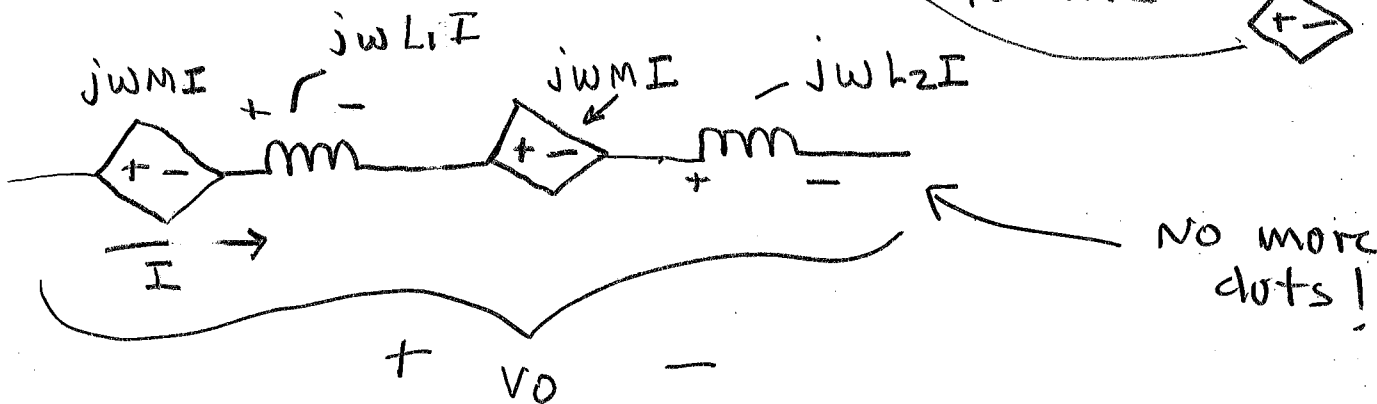
REVISIT THE SERIES COIL PROBLEM USING PHASORS

Find inductance of series combination



Current enters dot of L_2 so it makes dot of L_1 more positive

Current enters dot of L_1 so it makes the dot of L_2 more positive



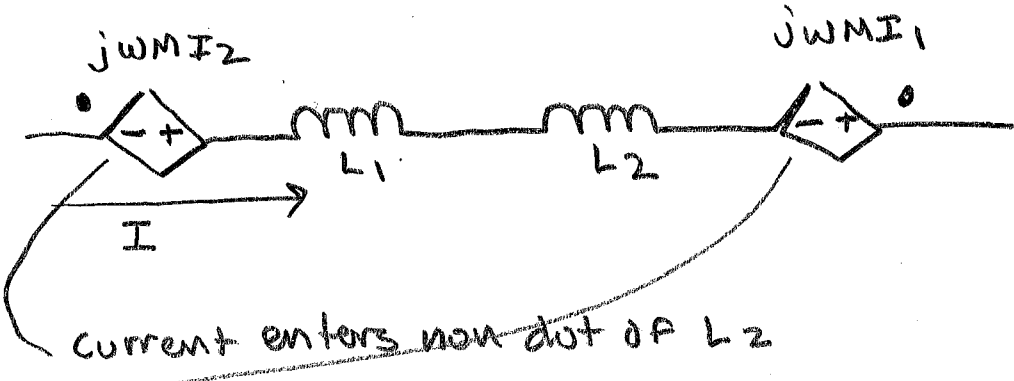
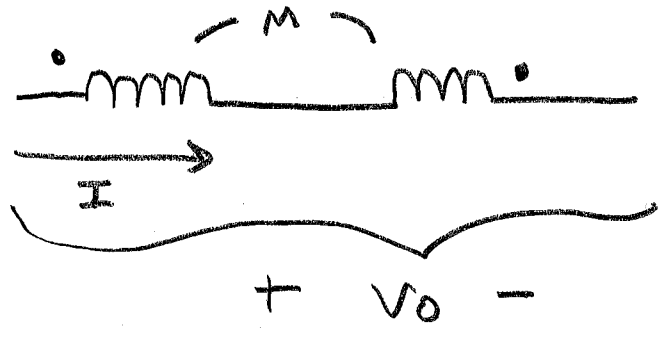
Add voltages starting at negative end -

$$V_0 = j\omega L_2 I + j\omega M I + j\omega L_1 I + j\omega M I$$

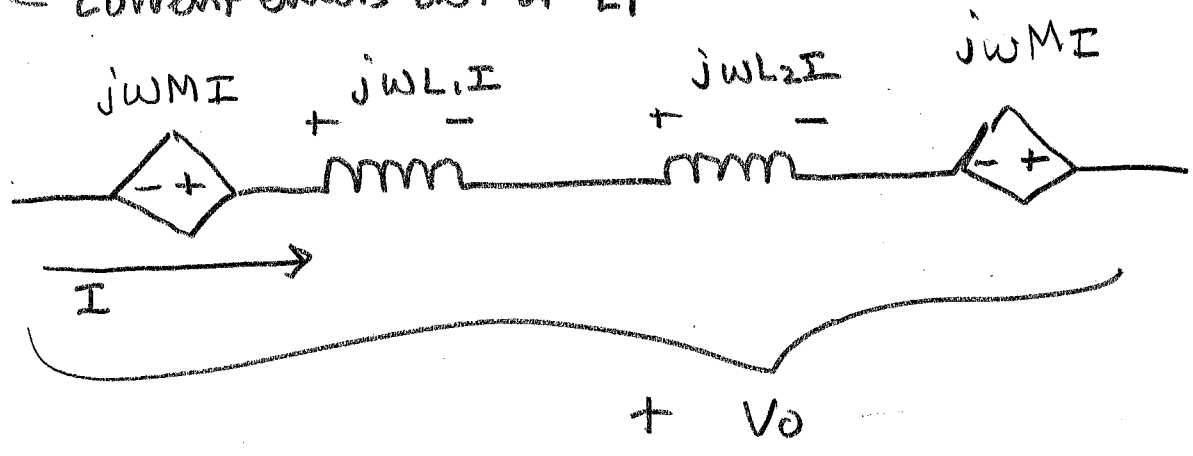
$$= j\omega I (L_1 + L_2 + 2M)$$

Equivalent inductance

Now Reverse dot on one coil and re-compute inductance,



Current enters dot of L1

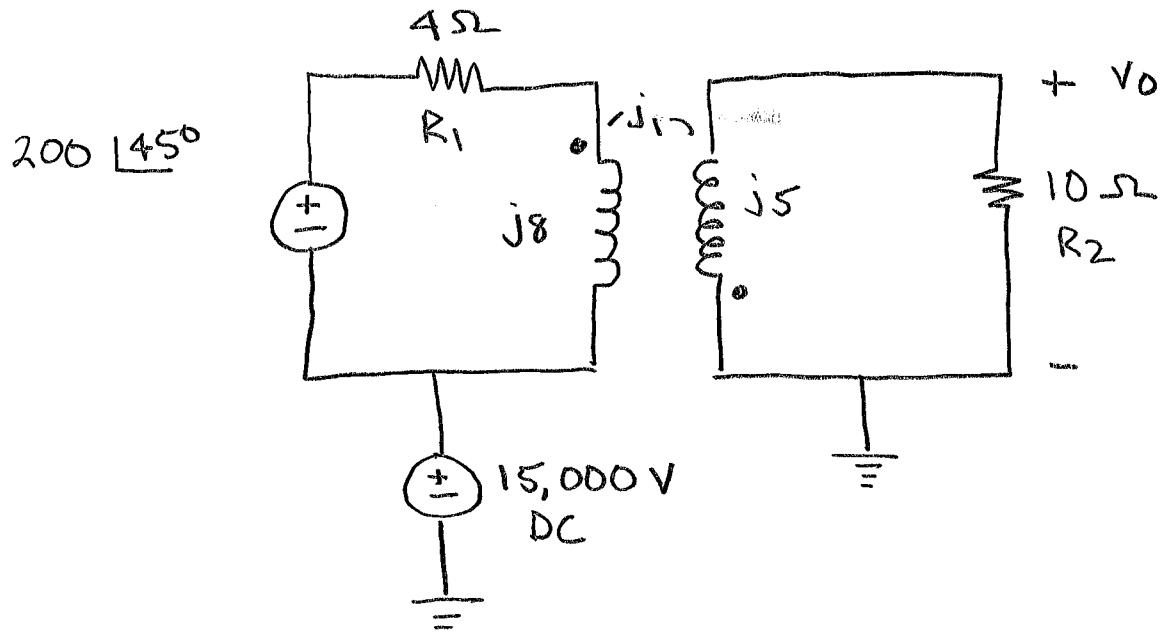


Add voltages starting at negative end,

$$V_0 = -j\omega M I + j\omega L_2 I + j\omega L_1 I - j\omega M I$$

$$V_0 = j\omega I (-M + L_2 + L_1 - M)$$

EQUIV INDUCTANCE



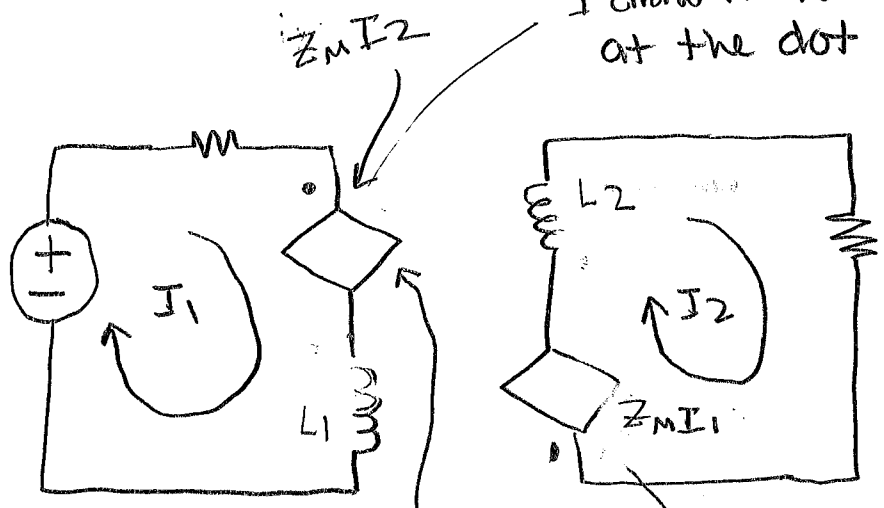
Find V_0

Strategy

- 1) Deal with the 15,000 volt source
- 2) Redraw with dependent sources
- 3) Use dots to establish polarity of dependent sources
- 4) Forget about the dots
- 5) Solve for I_1, I_2
- 6) $V_0 = I_2 \cdot 10\Omega$

Deal with DC

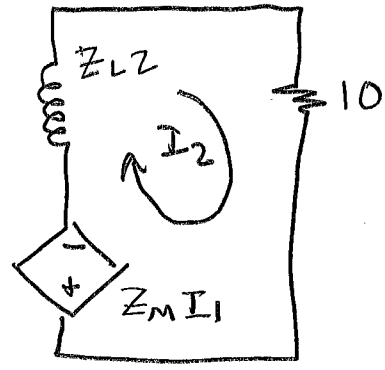
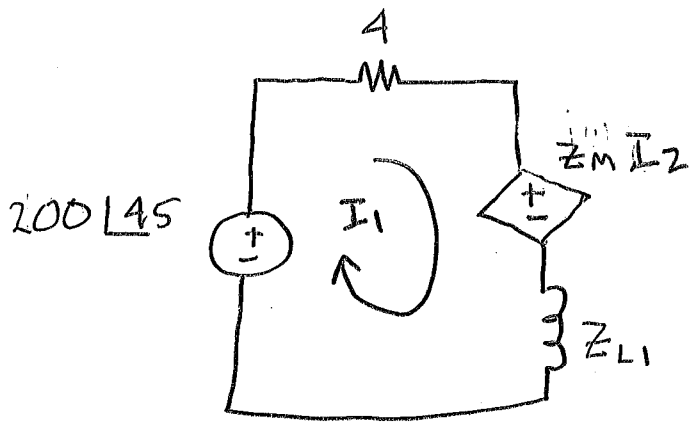
I draw the source at the dot



When I_1 goes into dot of L_1 it makes dot of L_2 more positive. so



When I_2 goes into dot of L_2 it makes dot of L_1 more positive so



$$\textcircled{1} \quad -V_s + 4I_1 + Z_M I_2 + Z_{L1} I_1 = 0$$

$$(4 + Z_{L1}) I_1 + Z_M I_2 = V_s$$

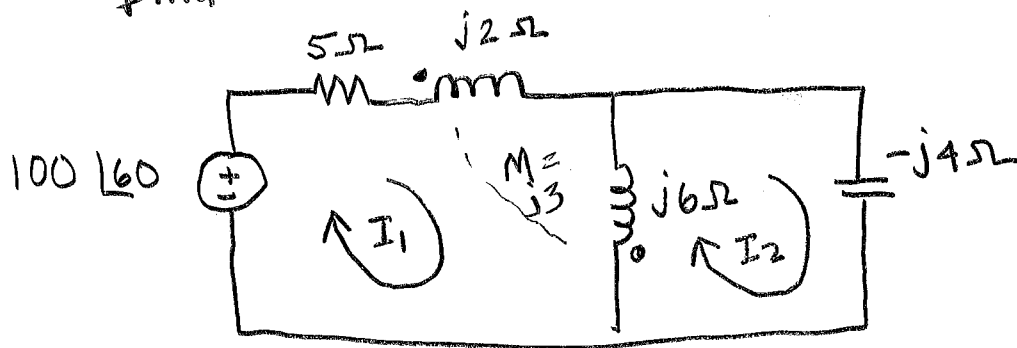
$$\textcircled{2} \quad Z_M I_1 + Z_{L2} I_2 + 10I_2 = 0$$

$$Z_M I_1 + (Z_{L2} + 10) I_2 = 0$$

$$\begin{bmatrix} 4 + Z_{L1} & Z_M \\ Z_M & Z_{L2} + 10 \end{bmatrix}^{-1} \begin{bmatrix} V_s \\ 0 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix} = \begin{bmatrix} 21.28 - j6.85 \\ -1.4 - j1.42 \end{bmatrix}$$

and $I_2 \times 10 = V_0 = (-1.4 - j1.42) \times 10 = 20 \angle -134^\circ$

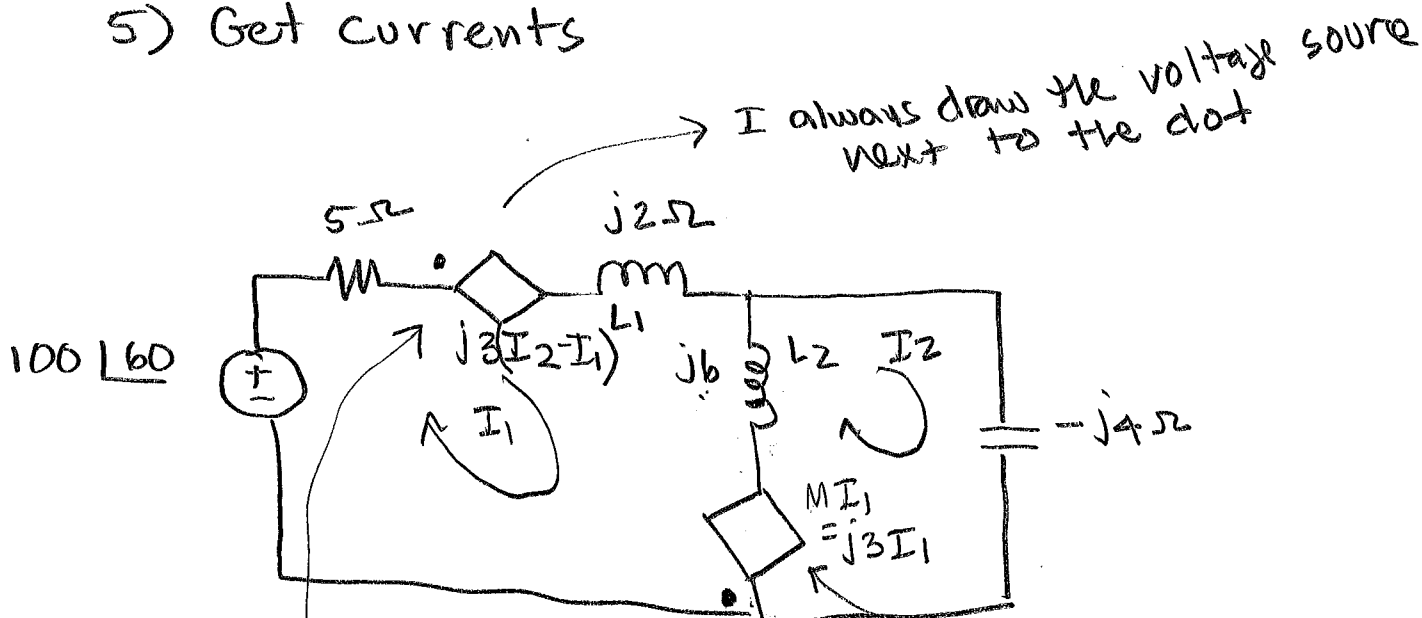
Find Mesh Currents



Practical Problem?

STRATEGY

- 1) Redraw with dependent sources
- 2) Use dots to establish polarity of dependent sources.
- 3) Forget about the dots
- 4) Write mesh equations
- 5) Get currents

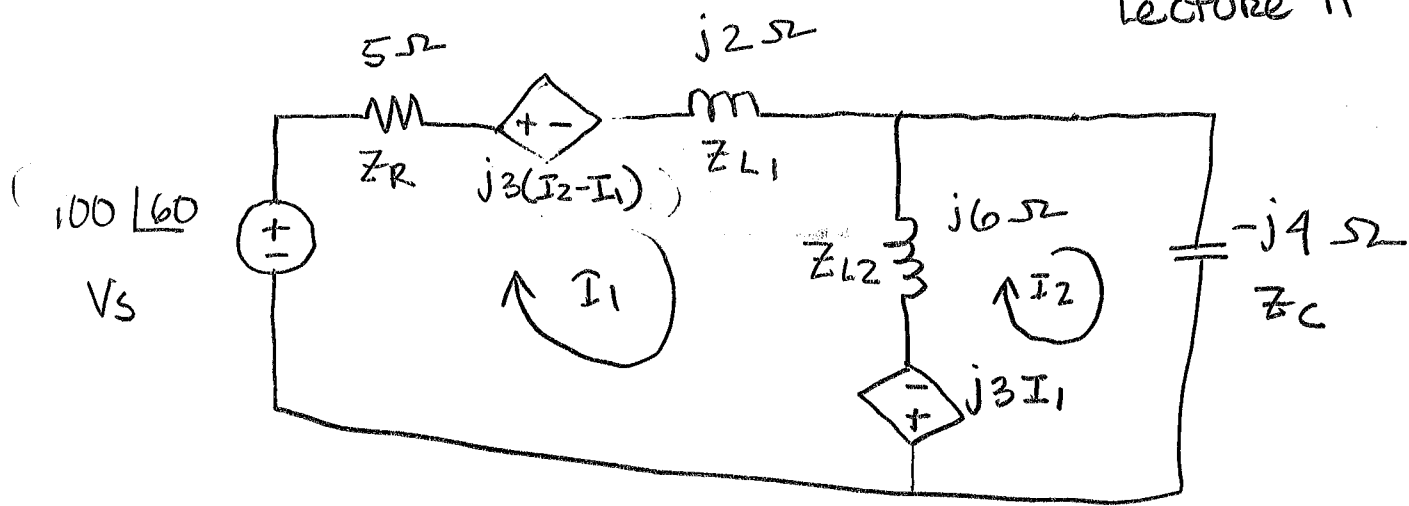


I_1 makes dot of L_2 more positive so



I_2 makes dot of L_1 more positive so





No more dots ↗

$$\textcircled{1} \quad -V_s + I_1 Z_R + Z_M(I_2 - I_1) + I_1 Z_{L1} + (I_1 - I_2) Z_{L2} - I_1 Z_M = 0$$

$$(Z_R + Z_{L1} + Z_{L2} - 2Z_M) I_1 + (Z_M - Z_{L2}) I_2 = V_s$$

$$\textcircled{2} \quad Z_M I_1 + (I_2 - I_1) Z_{L2} + I_2 Z_C = 0$$

$$(Z_M - Z_{L2}) I_1 + (Z_{L2} + Z_C) I_2 = 0$$

$$\begin{bmatrix} Z_R + Z_{L1} + Z_{L2} - 2Z_M & Z_M - Z_{L2} \\ Z_M - Z_{L2} & Z_{L2} + Z_C \end{bmatrix}^{-1} \begin{bmatrix} 100 \angle 60 \\ 0 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \end{bmatrix}$$

$$I_1 = 1.07 + j17.86 = 17.89 \angle 86.56$$

$$\textcircled{2} \quad I_2 = 1.61 + j26.78 = 26.83 \angle 86.56$$

SECTION 13.3 - Energy in a coupled circuit

eg 564 & 565 derive:

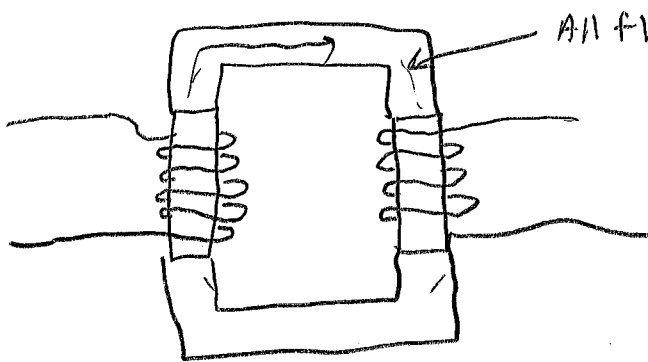
$$M_{12} = M_{21} = M \quad \text{EQ 13.30 a}$$

$$M \leq \sqrt{L_1 L_2} \quad \text{EQ 13.35 WITH PERFECT COUPLING}$$

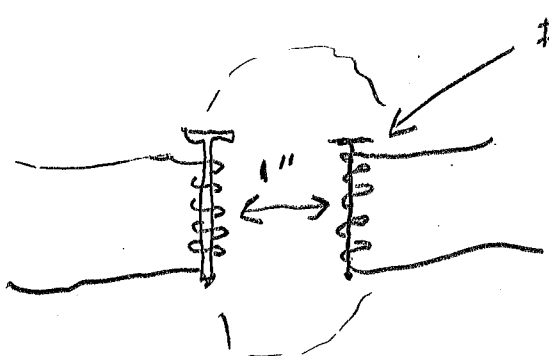
K = coefficient of coupling

$$K = \frac{M}{\sqrt{L_1 L_2}} \quad \text{EQ 13.36}$$

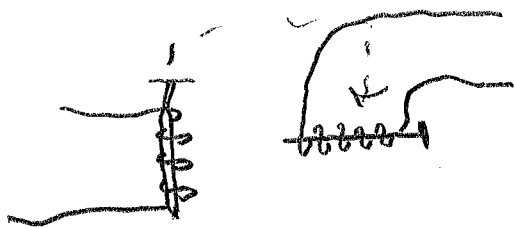
$$\text{SO } 0 \leq K \leq 1 \quad \text{OR } 0 \leq M \leq \sqrt{L_1 L_2}$$



IRON CORE $K \approx 1$
($M = \sqrt{L_1 L_2}$)



say $K \approx 0.5$



Fields orthogonal
no coupling $K=0$