

EXAM 1 REVIEW - EE-310

LECTURE #2

The Rules

2

"Verbal"

Equation

Inductor current cannot change instantaneously

$$i_L(0^+) = i_L(0^-) \quad (1)$$

Capacitor voltage cannot change instantaneously

$$V_C(0^+) = V_C(0^-) \quad (2)$$

Inductor voltage can change instantaneously

$$V_L = L \frac{di}{dt} \quad (3)$$

Capacitor current can change instantaneously

$$i_C = C \frac{dV}{dt} \quad (4)$$

At steady state $\frac{di}{dt} = 0$ so

inductor voltage is zero

$$V_L(\infty) = 0 \quad (5)$$

At steady state $\frac{dV}{dt} = 0$ so

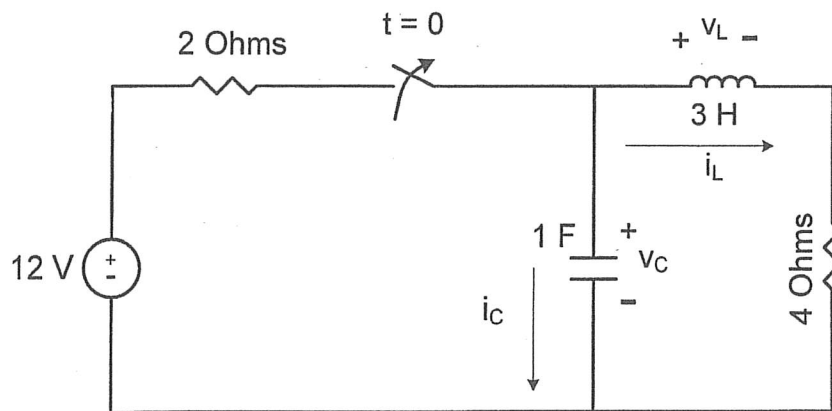
$i_C = 0$

$$I_C(\infty) = 0 \quad (6)$$

Name: DORR

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- 1) After being closed a long time, the switch opens at $t=0$. Find: (a) $v_C(0^+)$, (b) $i_C(0^+)$, (c) $dv_C/dt(0^+)$, (d) $v_L(0^+)$, (e) $i_L(0^+)$, (f) $dv_L/dt(0^+)$. (20%)



$$(3) \quad (a) \quad v_C(0^+) = \frac{4}{4+2} \times 12 = 8 \text{ V}$$

$$(4) \quad (b) \quad i_L(0^+) = i_L(0^-) = \frac{12}{4+2} = 2 \text{ A}, \quad i_C = -i_L = -2 \text{ A}$$

$$(4) \quad (c) \quad i_C = C \frac{dv}{dt}, \quad \frac{dv_C}{dt} = \frac{i}{C} = \frac{-2}{1} = -2 \text{ V/s}$$

$$(3) \quad (d) \quad \text{use KVL} \quad -v_C(0^+) + v_L(0^+) + 4 i_L(0^+) = 0$$

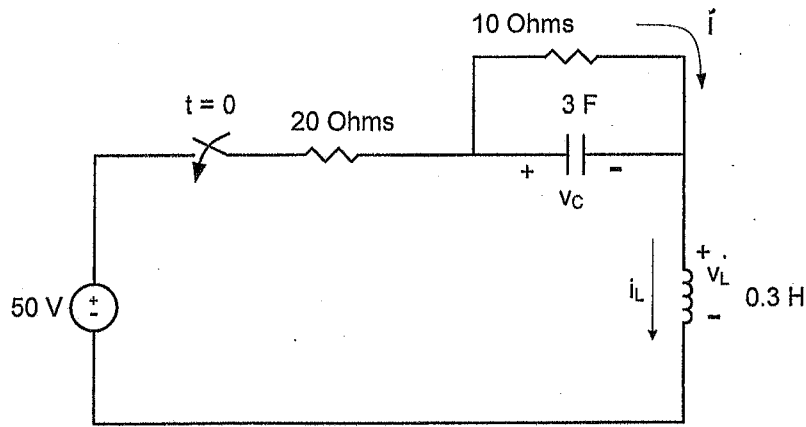
$$v_L(0^+) = v_C(0^+) - 4 i_L(0^+) = 8 - 4 \cdot (2) = 0 \text{ V}$$

$$(3) \quad (e) \quad i_L(0^+) = i_L(0^-) = 2 \text{ A (from part b)}$$

$$(3) \quad (f) \quad \text{Since } v_L(0^+) = 0 = L \cdot \frac{di_L}{dt}, \quad \frac{di_L}{dt} = \frac{di_R}{dt} = \frac{dv_R}{dt} = 0$$

$$\text{Therefore } \frac{dv_L}{dt} = \frac{dv_C}{dt} = -2 \text{ V/s}$$

2) After being ^{OPEN} closed a long time, the switch closes at $t=0$. Find: (a) $i(0^+)$, (b) $di/dt(0^+)$, (c) $i(\infty)$, (d) $dv/dt(0^+)$, (e) $i_L(0^+)$, (f) $di_L/dt(0^+)$ (g) $i_L(\infty)$, (15%)



(2) (a) inductor current can't change quickly so $i_L(0^+) = 0$
 \therefore no current in 20Ω , $3F$, or 10Ω and $i(0^+) = 0$.

(3) (b) $\frac{di}{dt}(0^+) = \frac{1}{R} \frac{dV_C(0^+)}{dt} = \frac{1}{R} \cdot \frac{i_L(0^+)}{C} = 0 \text{ A/s}$

(2) (c) $i_\infty = \frac{50}{10+20} = 1.67 \text{ A}$

(2) (d) $\frac{dV_C(0^+)}{dt} = \frac{i_C(0^+)}{C} = \frac{0}{C} = 0$

(2) (e) $i_L(0^+) = 0 \text{ A}$ (can't change inductor current quickly)

(2) (f) $\frac{di_L}{dt}(0^+) = \frac{50 \text{ V}}{0.3} = 166.7 \text{ A/s}$ \rightarrow No current so all voltage is across inductor

(2) (g) $i_L(\infty) = \frac{50}{20+10} = 1.66 \text{ A}$

Generalized responses

1/2

Over damped

$$r(t) = R_s + A_1 e^{s_1 t} + A_2 e^{s_2 t}$$

$$r(0^+) = R_s + A_1 + A_2$$

$$dr/dt(0^+) = A_1 s_1 + A_2 s_2$$

so

$$\begin{bmatrix} 1 & 1 \\ s_1 & s_2 \end{bmatrix} \begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \begin{bmatrix} r(0^+) - R_s \\ dr/dt(0^+) \end{bmatrix}$$

or

$$\begin{bmatrix} A_1 \\ A_2 \end{bmatrix} = \begin{bmatrix} 1 & 1 \\ s_1 & s_2 \end{bmatrix}^{-1} \begin{bmatrix} r(0^+) - R_s \\ dr/dt(0^+) \end{bmatrix}$$

Critically damped

$$r(t) = R_s + (A_1 + A_2 t) e^{-\alpha t}$$

$$r(0^+) = R_s + A_1$$

$$\frac{dr}{dt}(0^+) = -\alpha A_1 + A_2$$

$$\text{so } A_1 = r(0^+) - R_s$$

$$A_2 = \frac{dr}{dt}(0^+) + \alpha A_1$$

Underdamped

2/2

$$r(t) = R_s + (A_1 \cos(\omega_d t) + A_2 \sin(\omega_d t)) e^{-\alpha t}$$

$$r(0^+) = R_s + A_1$$

$$\frac{dr}{dt} = \frac{d}{dt} \left[R_s + A_1 \cos(\omega_d t) e^{-\alpha t} + A_2 \sin(\omega_d t) e^{-\alpha t} \right]$$

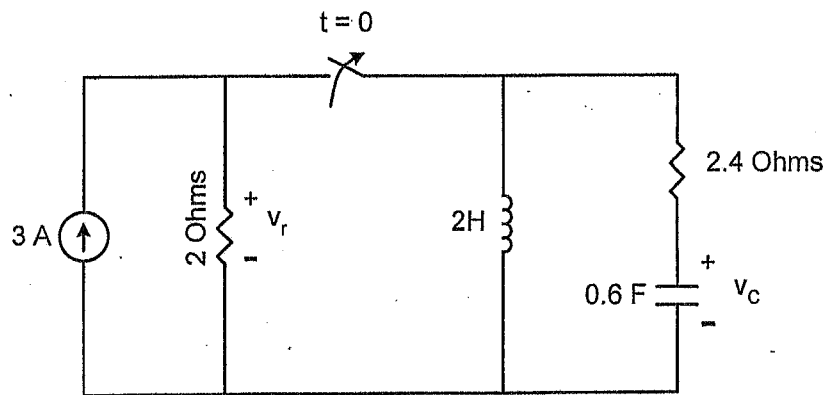
$$= -\alpha A_1 \cos(\omega_d t) e^{-\alpha t} - A_1 \omega_d \sin(\omega_d t) e^{-\alpha t} + A_2 \omega_d \cos(\omega_d t) e^{-\alpha t} - \alpha A_2 \sin(\omega_d t) e^{-\alpha t}$$

$$\frac{dr}{dt}(0^+) = -\alpha A_1 + A_2 \omega_d$$

$$\text{so } A_1 = r(0^+) - R_s$$

$$A_2 = \frac{\frac{dr}{dt}(0^+) + \alpha A_1}{\omega_d}$$

3) After being closed for a long time, the switch opens at $t=0$. Find: (a) $v_c(0^+)$, (b) $dv_c/dt(0^+)$, (c) $v_c(\infty)$, (d) $v_r(\infty)$, and (e) $v_c(t)$. (20%)



(3) (a) Inductor voltage at 0^- is 0 so $v_c(0^-) = v_c(0^+) = 0$

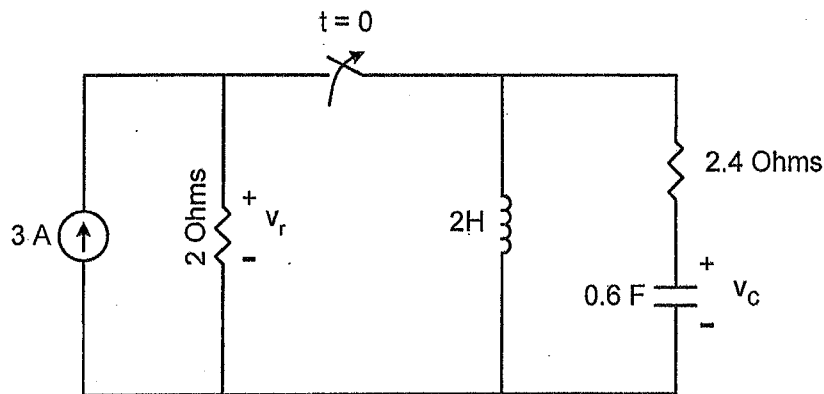
(3) (b) $i_L(0^-) = i_L(0^+) = 3A$, At $t=0^+$ Capacitor must supply current
 so $i_c(0^+) = -3A$, $\frac{dv_c}{dt}(0^+) = \frac{i_c(0^+)}{C} = \frac{-3}{0.6} = -5V/s$

(3) (c) $v_c(\infty) = 0$. All energy is dissipated

(3) (d) $V_R(\infty) = 3 \times 2 = 6V$

(Work part (e) on the next page)

Problem 3 (cont)



(e)

(1) $\alpha = R/2L = 0.6$

(1) $\omega_0 = \frac{1}{\sqrt{LC}} = \frac{1}{\sqrt{2 \times 0.6}} = 0.913$

(1) $\omega_d = \sqrt{\omega_0^2 - \alpha^2} = \sqrt{0.913^2 - 0.6^2} = 0.688 \text{ r/s}$

Since $\omega_0 > \alpha$ it is underdamped

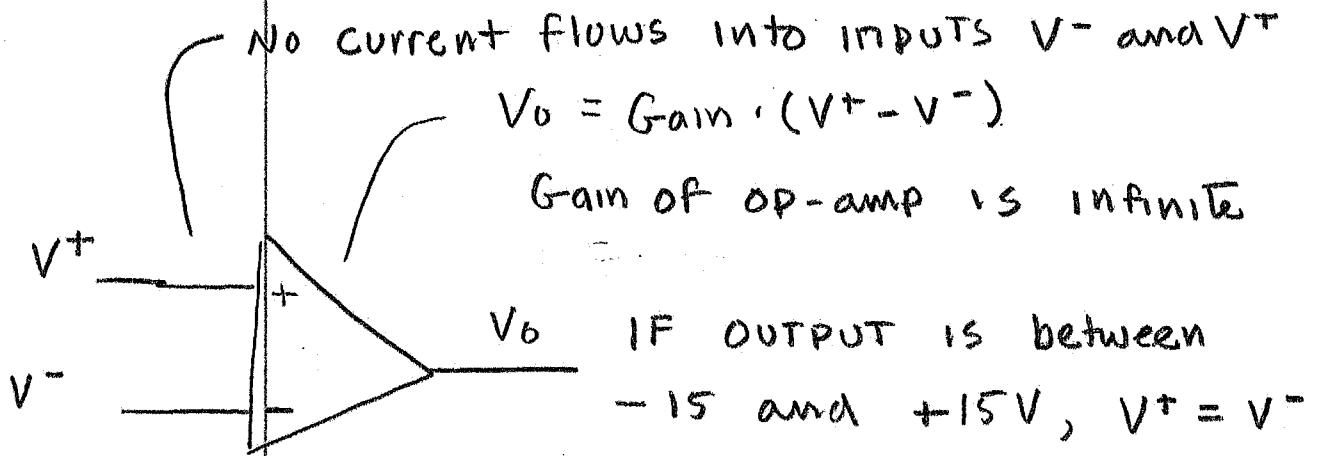
2 points for General formula $\rightarrow v_c(t) = e^{-\alpha t} (B_1 \cos(\omega_d t) + B_2 \sin(\omega_d t))$

(1) $B_1 = v_c(0^+) - v_c(\infty) = 0 - 0 = 0$

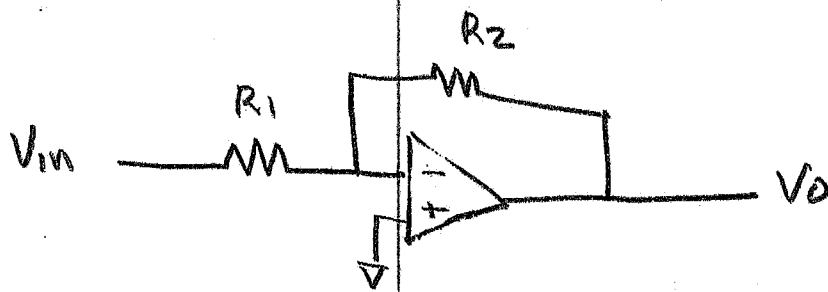
(1) $B_2 = \frac{\frac{dv_c(0^+)}{dt} + \alpha v_c(0^+)}{\omega_d} = \frac{-5 - 0}{0.688} = -7.27$

(1) $v_c(t) = -7.27 e^{-0.6t} \sin(0.688t)$

INTRODUCTION TO OP-AMPS FOR EE-310



Gain of op amp is infinite. What is the gain of this circuit?



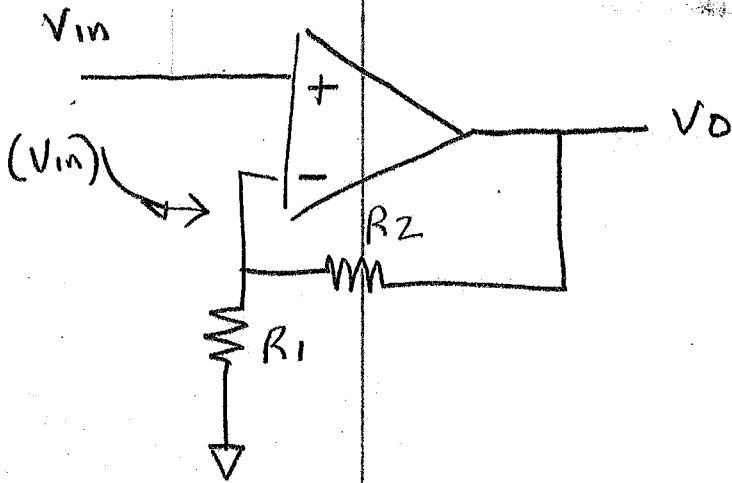
KCL at inverting terminal: (No current into V^-)

Also, since $V^+ = V^-$, $V^- = 0$

$$\frac{V_{in}}{R_1} + \frac{V_o}{R_2} = 0, \quad \frac{V_{in}}{R_1} = -\frac{V_o}{R_2} \quad \text{or} \quad \text{Gain} = \frac{V_o}{V_{in}} = -\frac{R_2}{R_1}$$

"Inverting Configuration"

What is the gain of this circuit?



Use KCL again. Remember $V^+ = V^- = V_{in}$

$$\frac{V_{in}}{R_1} = \frac{V_o - V_{in}}{R_2}$$

$$V_{in} R_2 = R_1 (V_o - V_{in}) = R_1 V_o - R_1 V_{in}$$

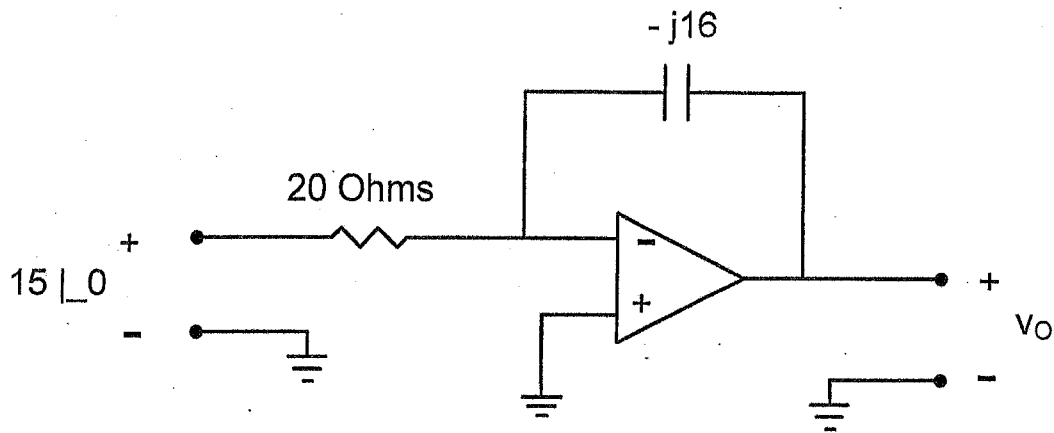
$$V_o R_1 = V_{in} R_2 + V_{in} R_1$$

$$V_o R_1 = V_{in} (R_2 + R_1)$$

$$\text{or } \frac{V_o}{V_{in}} = \text{Gain} = \frac{R_2 + R_1}{R_1}$$

"Non-inverting configuration"

6) Determine the output voltage for the circuit below. Express your result as a phasor in polar form. (15%)

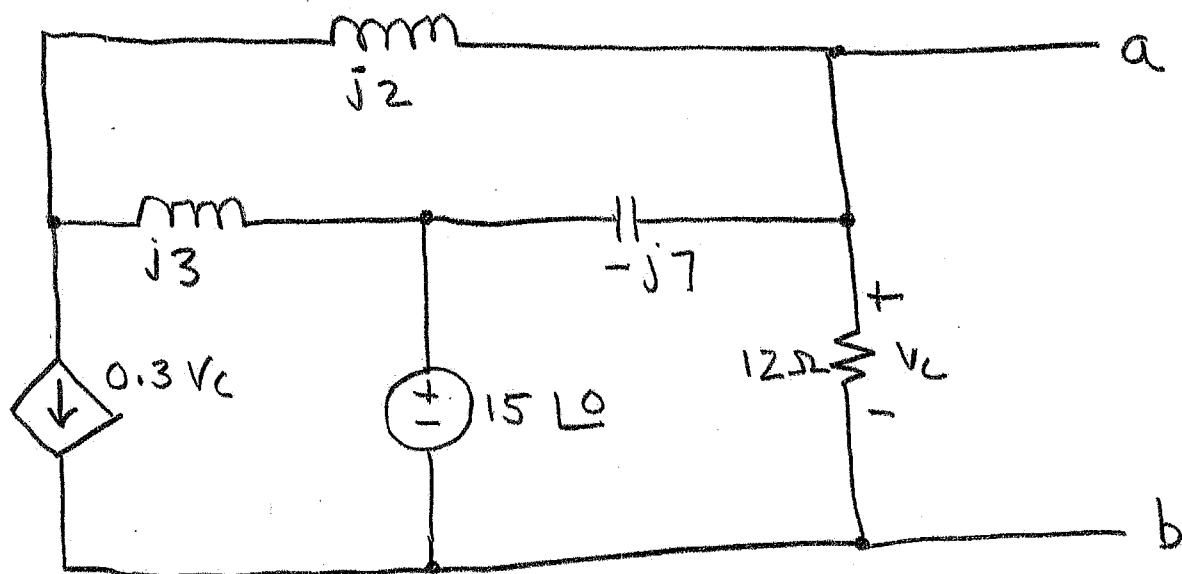


$$(8) \quad \frac{V_o}{V_{in}} = -\frac{Z_2}{Z_1}$$

$$(5) \quad V_o = V_{in} \cdot \left(-\frac{Z_2}{Z_1}\right) = 15\angle 0 \times \frac{-(-j16)}{20} = j12$$

$$(2) \quad V_o = 12\angle 90$$

Supplement for ASSIGN #5



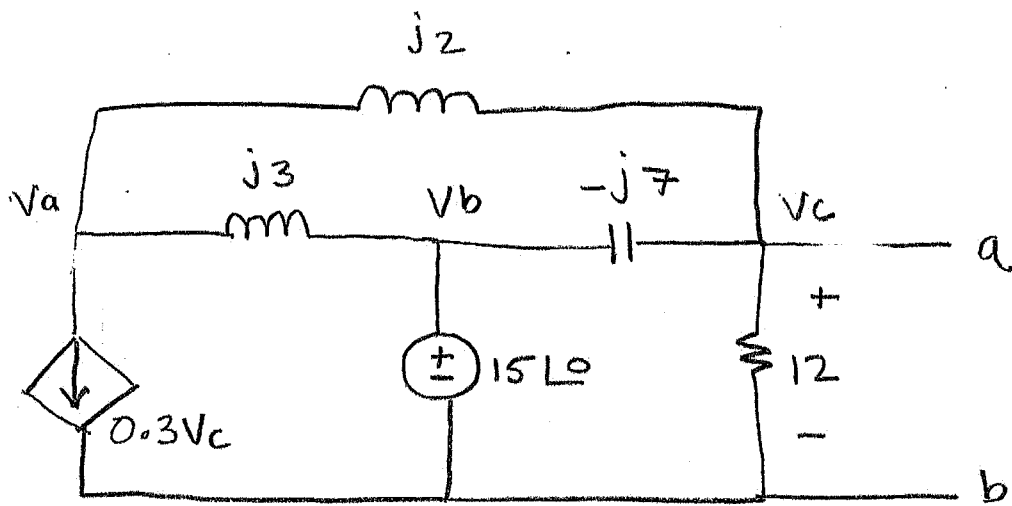
- 1) Determine the load that can be placed between terminals a and b that will receive maximum power transfer from the circuit.
- 2) Determine the power delivered to this load.

Hints: 1) Use KVL or KCL to get V_{TH}

2) For Thevenin impedance, see "case 2" on pg 140

3) I prefer getting Z_{TH} by computing I_{SC} then

$$Z_{TH} = \frac{V_{TH}}{I_{SC}}$$



Determine the Thevenin equivalent circuit using terminals a and b as the output

Use KCL:

Node voltage Va

$$(1) +0.3 V_c + \frac{(V_a - V_b)}{j3} + \frac{V_a - V_c}{j2} = 0$$

$$(1) \left[\frac{1}{j3} + \frac{1}{j2} \right] V_a - \frac{1}{j3} V_b + \left(+0.3 - \frac{1}{j2} \right) V_c = 0$$

Node voltage Vb

$$\hookrightarrow 1 + 15 \text{ V } \angle 0$$

Node voltage Vc

$$(2) \frac{V_c}{12} + \frac{V_c - V_b}{-j7} + \frac{V_c - V_a}{j2} = 0$$

$$\hookrightarrow \text{so } -\frac{1}{j2} V_a + \frac{1}{j7} V_b + \left(\frac{1}{12} + \frac{1}{-j7} + \frac{1}{j2} \right) V_c = 0$$

Substitute $V_b = 15 \angle 0$ into ① and ②

$$\textcircled{1} \left[\frac{1}{j3} + \frac{1}{j2} \right] V_a + \left[+0.3 - \frac{1}{j2} \right] V_c = \frac{15}{j3}$$

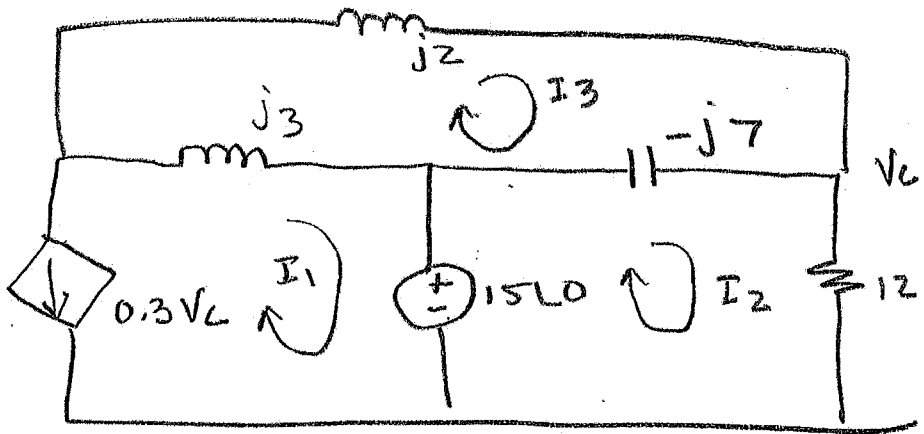
$$\textcircled{2} -\frac{1}{j2} V_a + \left[\frac{1}{12} + \frac{1}{-j7} + \frac{1}{j2} \right] V_c = -\frac{15}{j7}$$

Solving gives

$$V_a = 5.29 - j2.10$$

$$V_c = 0.6746 - j3.11 = V_{TH}$$

Now we'll use mesh analysis and see if we get the same voltage for V_c .



$$\textcircled{1} \quad I_1 = -0.3 V_C = -0.3 \times 12 I_2 \Rightarrow I_1 + 0.3 \times 12 I_2 = 0$$

$$\textcircled{2} \quad -15 + (I_2 - I_3) \times -j7 + I_2 \times 12 = 0$$

$$-15 - j7 I_2 + j7 I_3 + 12 I_2 = 0$$

$$(-j7 + 12) I_2 + j7 I_3 = 15$$

$$\textcircled{3} \quad (I_3 - I_2) \times -j7 + (I_3 - I_1) j3 + I_3 j2 = 0$$

$$-j3 I_1 + j7 I_2 + (j3 - j7 + j2) I_3 = 0$$

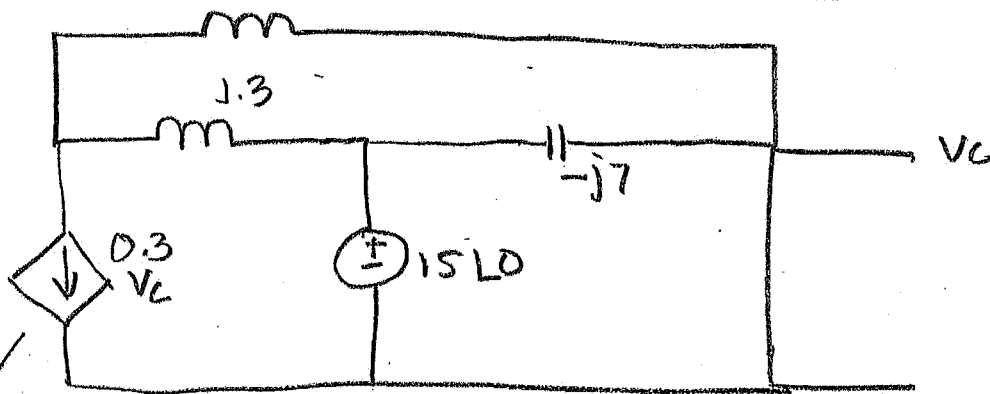
$$\begin{bmatrix} 1 & 0.3 \times 12 & 0 \\ 0 & -j7 + 12 & j7 \\ -j3 & j7 & j3 - j7 + j2 \end{bmatrix}^{-1} \begin{bmatrix} 0 \\ 15 \\ 0 \end{bmatrix} = \begin{bmatrix} I_1 \\ I_2 \\ I_3 \end{bmatrix}$$

$$12 I_2 = V_C = 0.6746 - j3.11 \text{ V} = V_{Th}$$

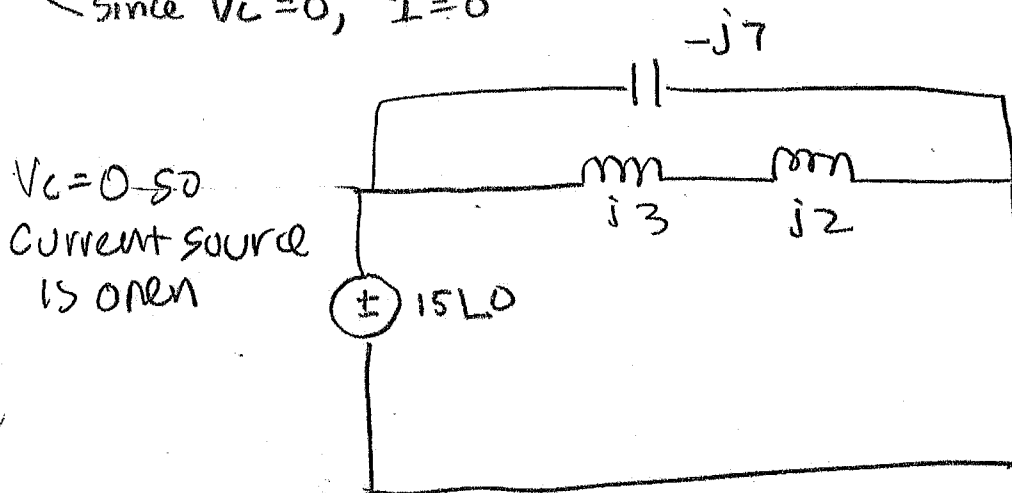
This agrees with mesh analysis

Get Z_{TH} $\xrightarrow{j2}$ Compute I_{SC} $Z_{TH} = \frac{V_{TH}}{I_{SC}}$

14



Since $V_L = 0$, $I = 0$



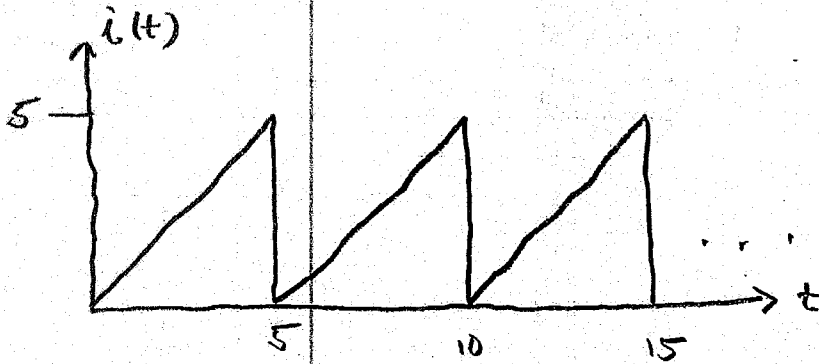
$V_L = 0$ so
current source
is open

$$I_{SC} = \frac{15 L_0}{-j7 \parallel j5} = \frac{15}{\frac{-j7 + j5}{35}} = \frac{15 \times -j2}{35} = \frac{-j30}{35} = -j0.857$$

$$\text{So } \frac{V_{TH}}{I_{SC}} = Z_{TH} = \frac{0.6746 - j3.11}{-j0.857} = \underbrace{3.63 + j0.787 \Omega}_{Z_{TH}}$$

DORR

11.27



$i(t)$ is a line (over one period)

so $i(t) = mt + b$ and $m=1$, $b=0$

$$i_{rms} = \left[\frac{1}{T} \int_0^T t^2 dt \right]^{1/2} = \left[\frac{1}{5} \left| \frac{t^3}{3} \right|_0^5 \right]^{1/2}$$

$$= \left[\frac{1}{5} \times \frac{5^3}{3} \right]^{1/2} = \sqrt{\frac{125}{15}} = 2.887A$$